TRANS CANADA HIGHWAY (TCH) KM 81+300 TO 85+500 ANIMAL UNDERPASS STRUCTURES GEOTECHNICAL SERVICES



REPORT

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TABLE OF CONTENTS

| 1.0 | ΙΝΤΙ | RODUC | | . I |
|-----|------|----------|--|-----|
| 2.0 | sco | PE OF | SERVICES | . I |
| 3.0 | PRO | JECT U | INDERSTANDING | . I |
| | 3.1 | Animal | Underpass Bridge at Km 83+090 (Wildlife Structure #1) | 2 |
| | 3.2 | | Underpass at Km 84+920 (Wildlife Structure #2) | |
| | 3.3 | | Underpass at Km 82+260 (Wildlife Structure #3) | |
| 4.0 | SITE | | TIGATION | . 2 |
| | 4.1 | Field In | vestigation | 2 |
| | 4.2 | Labora | tory Testing | 3 |
| 5.0 | SOIL | | GROUNDWATER CONDITIONS | . 3 |
| | 5.1 | EBA 20 | 010 Preliminary Geotechnical/Pavement Assessment Work | 3 |
| | 5.2 | | eted Soil Profile and Groundwater | |
| | | 5.2.1 | Animal Underpass Bridge at Km 83+090 (Wildlife Structure #1) | 4 |
| | | 5.2.2 | Animal Underpass at Km 84+920 (Wildlife Structure #2) | 4 |
| | | 5.2.3 | Animal Underpass at Km 82+260 (Wildlife Structure #3) | 5 |
| 6.0 | DES | IGN RE | COMMENDATIONS AND CONSTRUCTION CONSIDERATIONS | . 5 |
| | 6.1 | Animal | Underpass Bridge at Km 83+090 (Wildlife Structure #1) | 5 |
| | | 6.1.1 | Recommended Soil Design Parameters | |
| | | 6.1.2 | Bridge Foundations and Lateral Earth Pressure Coefficients | 6 |
| | | 6.1.3 | Frost Protection for Shallow Foundations | 6 |
| | | 6.1.4 | Construction Considerations | 7 |
| | 6.2 | Animal | Underpass at Km 84+920 (Wildlife Structure #2) | 7 |
| | | 6.2.1 | Recommended Soil Design Parameters | 7 |
| | | 6.2.2 | Underpass Foundation | 7 |
| | | 6.2.3 | Construction Considerations | 8 |
| | 6.3 | Animal | Underpass at Km 82+260 (Wildlife Structure #3) | 8 |
| | | 6.3.1 | Recommended Soil Design Parameters | 8 |
| | | 6.3.2 | Underpass Foundation | 9 |
| | | 6.3.3 | Global Stability of the Cut Slope | 9 |
| | | 6.3.4 | Construction Considerations | 9 |
| 7.0 | CLO | SURE | | 10 |

FIGURES

| Figure 1 | Key Plan |
|----------|---|
| Figure 2 | Borehole Locations - Underpass at Km 82+260 |
| Figure 3 | Borehole Locations - Bridge at Km 83+090 |

Figure 4 Borehole Locations - Underpass at Km 84+920

APPENDICES

- Appendix A EBA's General Conditions
- Appendix B Drawings Provided by McElhanney Consulting Services
- Appendix C Borehole Logs
- Appendix D Sieve Analyses Results

I.0 INTRODUCTION

EBA, a Tetra Tech Company (EBA) was retained by Parks Canada Agency (PCA) to carry out a geotechnical investigation at three proposed animal underpass structures including one bridge and two pipe-arch structures between Km 81+300 and 85+500 on the Trans Canada Highway (TCH) in Yoho National Park, BC. The purpose of this investigation was to determine the subsurface conditions at the proposed animal underpass sites, and provide geotechnical design recommendations for the foundations of the proposed structures. Based on information provided by McElhanney Consulting Services (MCS), we understand that the proposed bridge will be located at Km 83+090 (identified as Wildlife Structure #1), and the proposed pipe-arch structures will be located at Km. 84+920 and 82+260 (identified as Wildlife Structure #2 and 3).

This report provides the factual results of our geotechnical investigation and our geotechnical recommendations with respect to site preparation and foundation design for the proposed animal underpass structures.

The scope of this report is limited solely to the geotechnical aspects of the project.

2.0 SCOPE OF SERVICES

The scope of work for this project was described in EBA's proposal dated May 3, 2011 and includes:

- Site investigation and laboratory testing to determine soil conditions at the proposed animal underpasses;
- Provide recommendations for the bridge footing design parameters;
- Provide recommendations on spread footing foundations for the bridge including bearing capacity, sliding, settlement, ground preparation and geotechnical construction considerations;
- Provide recommendations on the bridge abutment backfill including lateral earth pressure coefficients, friction angle, unit weight and geotechnical construction considerations; and
- Provide geotechnical recommendation for the pipe-arch foundation design and geotechnical construction considerations.

3.0 **PROJECT UNDERSTANDING**

Drawings were provided by MCS which show the approximate footprints of the three animal underpass structures, preliminary design drawings for the crossing at Sta. 82+260 and a typical section for the proposed bridge. These drawings are included in Appendix B. The following sections outline EBA's understanding of the animal underpass structures based on these drawings.

3.1 Animal Underpass Bridge at Km 83+090 (Wildlife Structure #1)

The MCS drawings indicate that a new bridge will be constructed at Km 83+090. Based on the bridge cross section provided, the east and west bridge abutments are to be supported on strip footings. The strip footings are to be about 5.5 m wide, with an approximately 2 m high by 0.6 m wide reinforced concrete shear key.

The proposed abutment walls are 5 m high. Compacted granular structural fill will be placed at a 1H:1V slope behind the abutment walls from the inside edge of the strip footings. Compacted common fill will then be placed outside this zone. The final TCH grade will be raised by about 0.4 m at the bridge location.

3.2 Animal Underpass at Km 84+920 (Wildlife Structure #2)

The MCS drawings indicate that a new pipe-arch underpass will be constructed at Km. 84+920. EBA has not been provided with detailed information on this crossing structure such as length, invert elevation or typical cross sections; however we understand that it has a similar geometry to the typical cross section provided for the pipe-arch at Km 82+260 (Section 3.3).

Based on the road profile along the TCH (Appendix B) at the proposed underpass location, about 0.6 m of fill is proposed along the existing TCH to raise the grade at the center of the crossing to a final grade of El. 1607 m.

3.3 Animal Underpass at Km 82+260 (Wildlife Structure #3)

The MCS drawings indicate that a new pipe-arch will be constructed at Km 82+260. Based on the cross section provided, we understand that the crossing will be a 7.04 m wide by 4.06 m high corrugated steel plate pipe-arch. The bottom of the pipe-arch will be at about El. 1638.8 m at the north end, with a slope of 0.5% to the south. The total length of the steel pipe-arch is about 50.5 m. The pipe-arch will have up to 2 m of cover. It is understood that the existing TCH will be widened and raised with up to 2 m of fill placement. Since, the existing crossing is below the existing ditch elevation, cut slopes at 2H:1V will be developed for animal access, with a height of approximately 15.5 m to the north and 1 m to the south.

4.0 SITE INVESTIGATION

EBA conducted a geotechnical site investigation in order to assess the subsurface soil and groundwater conditions at the proposed animal underpass locations.

4.1 Field Investigation

The geotechnical field investigation was completed from June 13 to 16, 2011. Drilling was carried out using a truck mounted Becker Hammer (HAV 180 hammer) drill rig with a 170 mm outside diameter casing, supplied and operated by Beck Drilling and Environmental Services Ltd. from Calgary, Alberta. A total of seven (7) Becker open holes, and five (5) Becker closed holes were advanced at selected locations in the footprints of the proposed animal underpass structures. Where both open and closed holes were at the same location, they were drilled approximately 1 m apart. The open holes were carried out to obtain samples of the soils at various depths. The closed holes were used to measure the penetration resistance of the soils. Becker Hammer drilling was selected as it is able to penetrate course gravely and cobbley soils

which are typical of this area. Crossroads Traffic Control from Golden, BC provided traffic control during the field investigation.

Borehole locations were determined based on the drawings provided by MCS which show the proposed structures footprints (Appendix B). Boreholes were advanced on the shoulder or outer lane of the TCH on each side of the proposed crossings. Figures 2 through 4 show the drilled borehole locations which were surveyed by MCS.

Standard Penetration Tests (SPTs) were performed at the proposed bridge location in two Becker open holes (BH2011-03 and BH2011-04) using an automatic trip hammer. SPT testing was limited due to the gravel and cobbles that were encountered, which obstruct the SPT sampler.

Upon completion of the drilling, all boreholes were backfilled with bentonite chips to approximately 1.5 m depth below the existing ground level, followed by approximately 1 m of sand, a 0.3 m concrete plug and an asphalt patch.

EBA's field engineer provided full-time supervision of the drilling which included logging and sampling of the soils, recording the Becker hammer blows per foot for closed ended drill casing and recording SPT data. Details of the subsurface soil and groundwater conditions are presented in the borehole logs in Appendix C.

4.2 Laboratory Testing

Selected soil samples collected from the drilling were brought to EBA's laboratory for further examination, classification and index testing. Lab tests including moisture contents, grain size analyses and a hydrometer were performed on selected samples from the boreholes. Moisture content and hydrometer results presented on the borehole logs in Appendix C, and grain size distribution results are summarized in Appendix D.

5.0 SOIL AND GROUNDWATER CONDITIONS

5.1 EBA 2010 Preliminary Geotechnical/Pavement Assessment Work

EBA undertook a previous geotechnical investigation on the TCH between Km 82+000 and 88+000 in October 2010 to obtain shallow soil conditions and pavement thickness information using test pits and auger drilling. Information on soil conditions from this investigation are summarized in EBA's previous report entitled "Geotechnical and Pavement Assessment, Trans Canada Highway Twinning Project, Alberta and British Columbia, Canada" (2010). The test pit and borehole information from this study in the vicinity of the proposed animal underpasses show that soil conditions consist of sand and gravel mixtures with variable amounts of cobbles and boulders. Layers of silt and clayey silt up to 0.5 m thick were encountered at two locations near the proposed underpasses. However, these layers were in the upper 1.5 m of the soil profile, therefore they will likely be removed prior to construction of the structures and will not influence the design.

5.2 Interpreted Soil Profile and Groundwater

5.2.1 Animal Underpass Bridge at Km 83+090 (Wildlife Structure #I)

Boreholes BH2011-03 and BH2011-04 were drilled by EBA in 2011 near the east and west abutments of the proposed bridge at Km 84+920. Borehole BH2011-03 is located near the west abutment on the south side of the existing TCH eastbound lane, and borehole BH2011-04 is located near the east abutment on the north side of the existing TCH westbound lane. Borehole locations are shown in Figure 3.

The ground conditions encountered at the west abutment of the proposed bridge consisted of gravelly sand to a depth of about 0.6 m below existing ground, overlying sand and gravel to a depth of about 4.6 m, overlying compact to <u>dense gravelly sand with cobbles to a depth of about 8.2 m</u>, overlying sandy gravel with cobbles to the depth of termination of borehole BH2011-03 at 10.1 m. Groundwater was not encountered at BH2011-03 during the field investigation.

The ground conditions encountered in the east abutment of the proposed bridge consisted of 140 mm of asphalt overlying loose to compact gravelly sand to a depth of about 4 m below existing grade, overlying compact medium to coarse sand, some gravel to a depth of about 4.9 m, overlying compact coarse sand with cobbles to a depth of about 6.7 m, overlying compact to dense gravelly sand, some silt with lenses of brown silty clay to the depth of termination of the Becker open hole BH2011-04 at 8.3 m. The closed Becker hole BH2011-04 penetrated to a depth of refusal at 10.1 m. Becker penetration rates of 7 to 21 blows per 0.3 m at depths between 8 m and 8.9 m depth are considered to be loose to compact. However, based on the soil conditions encountered at the bottom of the open hole BH2011-04, this layer is likely to be weathered till-like material or rock.

Moisture contents of the soils encountered at this location ranged from 1.4% to 5.9%. Groundwater was encountered at about 9.8 m below existing grade in BH2011-04.

5.2.2 Animal Underpass at Km 84+920 (Wildlife Structure #2)

Boreholes BH2011-01 and BH2011-02 were drilled by EBA in 2011 in the vicinity of the proposed animal underpass at Km 84+920. Borehole BH2011-01 is located on the south side of the existing TCH eastbound lane, and borehole BH2011-02 is located on the north side of the existing TCH westbound lane. Borehole locations are shown in Figure 4.

The ground conditions encountered in the south side of the proposed pipe-arch (refer to BH2011-01) consisted of 150 mm of asphalt overlying compact gravel and sand, some silt to a depth of about 1.5 m below existing grade, overlying dense to very dense sand, some silt, some gravel with cobbles to a depth of about 7 m, overlying loose to dense gravelly sand to a depth of about 8.3 m, overlying very dense sandy gravel to a depth of about 9.1 m, overlying dense to very dense silty sand and gravel to a depth of about 12.2 m, overlying dense to very dense sand to the depth of termination of 15 m. Moisture contents of the soils encountered in borehole BH2011-01 ranged from 3% to 12%, with increasing moisture content with depth.

The ground conditions encountered in the north side of the proposed pipe-arch also consisted of 150 mm of asphalt overlying sand and gravel, some silt with cobbles to a depth of about 6.4 m below existing grade, overlying silt and sand to a depth of about 8.2 m, overlying sand with cobbles to a depth of about 11.9 m,

overlying sand with thin lenses of silt to a depth of about 12.8 m, overlying sand and silt (Till-like) to the depth of termination at 13.4 m.

Moisture contents of the soils encountered in borehole BH2011-02 ranged from 5% to 13%, and exhibit increasing moisture content with depth. Groundwater was not observed in either borehole.

5.2.3 Animal Underpass at Km 82+260 (Wildlife Structure #3)

Boreholes BH2011-05, BH2011-06 and BH2011-07 were drilled by EBA in 2011 in the vicinity of the proposed animal underpass at Km. 82+260. Borehole BH2011-05 is located on the north side of the existing TCH westbound lane, and boreholes BH2011-06 and BH2011-07 are located on the south side of the existing TCH eastbound lane. Borehole locations are shown in Figure 2.

The ground conditions encountered at the north side of the proposed underpass consisted of 160 mm of asphalt overlying dense sand and gravel to gravelly sand, becoming compact at 2 m, becoming very dense from 2.7 m to the termination depth of 3.9 m. Cobbles are inferred to be present within the native soil deposits. Two boreholes (BH2011-06 and BH2011-07) were drilled on the south side of the proposed underpass at Km 82+260. The ground conditions consisted of compact sand and gravel to gravelly sand to a depth of about 0.8 m becoming dense and extending to the depth of termination. BH2011-06 and BH2011-7 were terminated at depths of 4.2 m and 3.9 m below existing grade due to refusal. Cobbles are inferred to be present.

Moisture contents of the soils encountered at this location ranged from 2% to 6%. Groundwater was encountered at 3.7 m below the existing grade in BH2011-05 and BH2011-06, and 4 m in BH2011-07.

It is expected that drill refusal was encountered on a boulder layer within the soil profile, however there is potential that bedrock exists near surface which would likely prevent installation of the underpass structure. Construction challenges should also be expected if a boulder layer is present at depth.

6.0 DESIGN RECOMMENDATIONS AND CONSTRUCTION CONSIDERATIONS

6.1 Animal Underpass Bridge at Km 83+090 (Wildlife Structure #1)

6.1.1 Recommended Soil Design Parameters

The recommended foundation design parameters in Table 1 represent the average soil parameters below the base of the footings. The groundwater table was estimated to be 5 m below the base of the bridge footings.

| Table 1: Recommended Soil Desig | ın Parameters – Animal Underr | bass Bridge at Km | 84+920 |
|---|---|------------------------------|--------------------------|
| Parameter | Natural Foundation Soil (Compact Sand, Some Gravel to Gravelly) | Structural Fill ¹ | Common Fill ² |
| Bulk unit weight, γ (kN/m ³) | 20 | 21 | 20 |
| Effective cohesion, c' (kPa) | 0 | 0 | 0 |
| Effective friction angle, ϕ' (degree) | 35 | 38 | 34 |

¹ Recommended backfill parameters to be used within the 1H:1V zone behind the abutments.

² Recommended backfill parameters for fill outside the 1H:1V zone behind abutments.

6.1.2 Bridge Foundations and Lateral Earth Pressure Coefficients

It is understood that shallow foundations (strip footings of 5.5 m width with a 2 m deep shear key at the edge of the footings furthest from the overpass) are the preferred foundation option for the proposed bridge abutments. The bridge footings will be founded on native compact sand with gravel at about El. +1641 m. It is understood that footings will be placed on about 0.6 m of structural fill bedding.

The factored bearing resistance of the proposed bridge foundations (strip footings of width 5.5 m) is <u>300 kPa</u> assuming a geotechnical resistance factor of 0.45. This bearing resistance is based on the serviceability limit state and assumes that 35 mm of bridge abutment settlement can occur. Much of this settlement will occur during loading of the foundations. Maximum differential settlements of 15 mm are expected.

Active, at-rest and passive earth pressures acting on the abutments have been calculated assuming that the backfill is common fill ($\phi' = 34$ degrees). The static earth pressure coefficients for active, at-rest and passive conditions are estimated to be about 0.27, 0.43 and 3.7, respectively. Passive earth pressure should only be applied to the shear key and neglected for footings embedment. It should be noted that fairly large movements will be required to mobilize the full passive earth pressure against the shear key. A compaction surcharge should only be applied if the abutments are considered rigid. A live load surcharge equal to an equivalent additional fill height of 0.8 m (as per Clause 6.9.5, Canadian Highway Bridge Design Code (CHBDC) CAN/CSA-S6-06) should be applied.

Sliding and overturning of the proposed bridge foundations were analysed using the typical bridge cross section provided by MCS. In the sliding analysis, the ultimate sliding friction angle along the interface between the strip footings and the foundation soil was taken as 0.8 of foundation soil internal friction angle (CHBDC, 2006). The analyses indicate that bridge foundations have static factor of safety values against overturning and sliding greater than 1.5.

6.1.3 Frost Protection for Shallow Foundations

A frost penetration depth of 2.5 m is anticipated for the site. It is expected that this depth of frost penetration may occur in open areas with little to no snow cover. Therefore, it is recommended that shallow foundations be place at a minimum depth of 2.5 m to provide frost protection.

If footings are not provided with this amount of soil cover, the use of insulation or placement of non-frost susceptible soil under the footings should be considered.

6.1.4 Construction Considerations

Soft or wet materials or areas with organic or other unsuitable material should be removed and backfilled with structural fill below the footprint of the proposed bridge footings and behind the abutments. The structural fill should be compacted to 98% of the Standard Proctor Maximum Dry Density (SPMDD). All subgrade should be proof-rolled and reviewed by a geotechnical engineer prior to footing installation.

It is recommended that well graded crushed granular material with less than 8% fine content (particles less than 0.075 mm diameter) be used as structural fill behind the abutment. Common fill behind this structural fill should be free draining granular material. Embankment fills (structural and common fills) should be compacted to 98% of SPMDD at +/- 2% of the optimum moisture content. All lifts should have a maximum 300 mm loose lift thickness. Proper drainage should be provided behind the abutment to reduce hydrostatic pressures.

All temporary excavation should be carried out in accordance with WorkSafe BC Occupational Health and Safety (OHS) Regulations. Surface water should be directed away from excavations. Stockpiling or storage of excavation spoils, construction materials or heavy equipment should not be permitted within 2 m of the crest of any excavation or trench to reduce the potential for slope instability.

Based on the groundwater level information at the proposed bridge location, groundwater is not expected to be an issue for shallow excavations in natural soils. If soil or groundwater conditions vary from those on which our recommendations are based, EBA should review the excavation plan prior to proceeding with construction.

6.2 Animal Underpass at Km 84+920 (Wildlife Structure #2)

6.2.1 Recommended Soil Design Parameters

Based on the results of the field investigation and laboratory testing, recommended soil design parameters are presented in Table 2.

| Parameter | Natural Foundation Soil (Dense to Very Dense Sand and Gravel to Sand, some Gravel) | Common Fill ¹ |
|---|---|--------------------------|
| Bulk unit weight, γ (kN/m ³) | 21 | 20 |
| Effective cohesion, c' (kPa) | 0 | 0 |
| Effective friction angle, ϕ' (degree) | 38 | 34 |

Table 2: Recommended Soil Design Parameters – Animal Underpass at Km 84+920

¹ Recommended construction backfill parameters to be used in the vicinity of the pipe-arch.

6.2.2 Underpass Foundation

We understand that the underpass layout at this location is similar to the animal underpass at Km 82+260. Based on the subsurface soil conditions encountered at boreholes BH2011-01 and BH2011-02, the proposed underpass will likely be founded on dense to very dense sand and gravel. About 0.75 m to 2 m of fill is to be placed above the underpass crown. It is assumed that the grade of the TCH will be raised by approximately 0.6 m.

Installation of the underpass at the proposed grade will reduce the ground pressure at the footing level. Given the reduction in ground pressure at the foundation level and the height of the underpass, bearing capacity and settlement are not considered to be a significant issue for the static case.

Active, at-rest and passive earth pressures acting on the pipe-arch have been estimated assuming that the fill surrounding the pipe-arch is compacted common fill ($\phi' = 34$ degrees). The static earth pressure coefficients for active, at-rest and passive conditions are estimated to be about 0.28, 0.44 and 3.5, respectively.

6.2.3 Construction Considerations

Soft or wet materials exposed on the subgrade should be removed and replaced with suitable granular fill within the footprint of the proposed pipe-arch foundation. Exposed loose granular material should be compacted to 98% of SPMDD. In the backfill area and above the pipe, fill material and compaction shall comply with the pipe-arch supplier's specification. Next to the proposed underpass, a temporary cut will be required. All temporary excavation and cut slopes should be carried out in accordance with WorkSafe BC Occupational Health and Safety (OHS) Regulations. Surface water should be directed away from the excavation. Stockpiling or storage of excavation spoils, construction materials or heavy equipment should not be permitted within 2 m of the crest of any excavation or trench to reduce the potential for slope instability.

Based on the groundwater information at this proposed animal underpass location, groundwater seepage may be observed in shallow excavations. If soil or groundwater conditions vary from those on which our recommendations are based, EBA should review the excavation plan prior to proceeding with construction.

6.3 Animal Underpass at Km 82+260 (Wildlife Structure #3)

Due to the shallow depth of water encountered within the boreholes drilled at this crossing location, as well as the potential bedrock/boulder layer at depth, installation of this animal underpass may be problematic. If the water observed within the boreholes represents the groundwater table, then the base of the animal underpass structure will be below water and the location of the crossing may need to be revised. Alternatively the proposed base of the underpass could be raised. The highway grade could also be raised or separate drainage culverts could be installed at elevations lower than the underpass.

Prior to construction of an animal underpass at this location, it is recommended that further investigation is undertaken in order to confirm the static groundwater level, as well as the refusal material at depth.

The recommendations below assume that the water observed was not the regional ground water table and that the ground water table is lower than observations made during drilling.

6.3.1 Recommended Soil Design Parameters

Recommended values of soil design parameters are presented in Table 3.

| Table 3: Recommended Soil Design Parameters – Animal Underpass at Km. 82.260 | | | | | | | | | | | | |
|--|--|--------------------------|--|--|--|--|--|--|--|--|--|--|
| Parameter | Natural Foundation Soil (Dense to Very Dense Sandy Gravel to Gravelly Sand) | Common Fill ¹ | | | | | | | | | | |
| Bulk unit weight, γ (kN/m ³) | 21 | 20 | | | | | | | | | | |
| Effective cohesion, c' (kPa) | 0 | 0 | | | | | | | | | | |
| Effective friction angle, ¢' (degree) | 38 | 34 | | | | | | | | | | |

¹ Recommended construction backfill parameters to be used in the vicinity of the underpass.

Underpass Foundation 6.3.2

It is expected that the proposed pipe-arch will likely be founded on a dense to very dense sandy gravel layer to the north and a gravelly sand layer to the south. The grade of the existing TCH will be raised by 0.2 m in the area of the crossing. For the purpose of road widening, a thickness of 2 m and 1.25 m of granular fill will be placed on existing grade at the south and north ends of the pipe, respectively.

Installation of the pipe-arch at the proposed grades will reduce the ground pressure at the foundation level when compared to the existing condition. Given the reduction in ground pressure at the foundation level and the depth of the pipe, bearing capacity and settlement are not likely to be a concern.

Active, at-rest and passive earth pressures acting on the pipe-arch have been calculated assuming that the fill on the side of the pipe is compacted engineered fill ($\phi' = 34$ degrees) as per the pipe-arch supplier's specifications. The static earth pressure coefficients for active, at-rest and passive conditions are estimated to be about 0.28, 0.44 and 3.5, respectively.

6.3.3 **Global Stability of the Cut Slope**

Excavation is required at both ends of the underpass to create animal access. It is understood that these slopes will be a maximum of 2H:1V, with a height of approximately 15.5 m and 1 m at the north and south ends respectively.

Based on the results of the field investigation and laboratory testing, the proposed access cut slopes will be within sand and gravel containing cobbles and boulders. Existing slopes in the area are approximately 2H:1V or slightly flatter at the north end of the underpass and are showing no visible signs of instability. The proposed slopes of 2H:1V are considered acceptable based on the available information. A number of large (>1 m diameter) boulders were observed on the surface of the slope, which could lead to challenges during excavation.

Construction Considerations 6.3.4

Soft or wet materials exposed within the subgrade or organic or other unsuitable material should be removed and replaced with approved granular fill within the footprint of the proposed underpass foundation. Loose granular material should be compacted to 98% of Standard Proctor Maximum Dry Density (SPMDD). All subgrade should be reviewed by a geotechnical engineer prior to pipe-arch installation.

A gasket or other seal should be installed in the joints of the individual pipe-arch sections to avoid migration of fines into the underpass. Alternatively, filter cloth could be placed against all joints on the outside of the pipe-arch. In backfill areas, fill material and compaction shall be in accordance with pipearch supplier specifications. Outside the pipe-arch backfill zone, fill should be compacted to 98% of SPMDD and within 2 percent of optimum moisture. Lifts should be 300 mm or less in thickness.

All temporary excavation and the proposed cut slopes should be carried out in accordance with WorkSafe BC Occupational Health and Safety (OHS) Regulations. Surface water should be directed away from the excavation; temporary dewatering may be required. Stockpiling or storage of excavation spoils, construction materials or heavy equipment should not be permitted within 2 m of the crest of any excavation or trench to reduce the potential for slope instability.

Based on the water level observed during drilling, groundwater issues are expected during construction and in the long term. A design that addresses ground water above the proposed pipe arch invert is recommended.

Excavation of the proposed cut slopes should proceed from the top down. Final excavation plans should be reviewed by EBA. Both temporary and permanent cut slopes should be inspected by EBA to confirm that the soil and groundwater conditions are as anticipated.

7.0 CLOSURE

We trust this report meets your present requirements. Should you have any questions or comments, please contact the undersigned at your convenience.

EBA, A Tetra Tech Company

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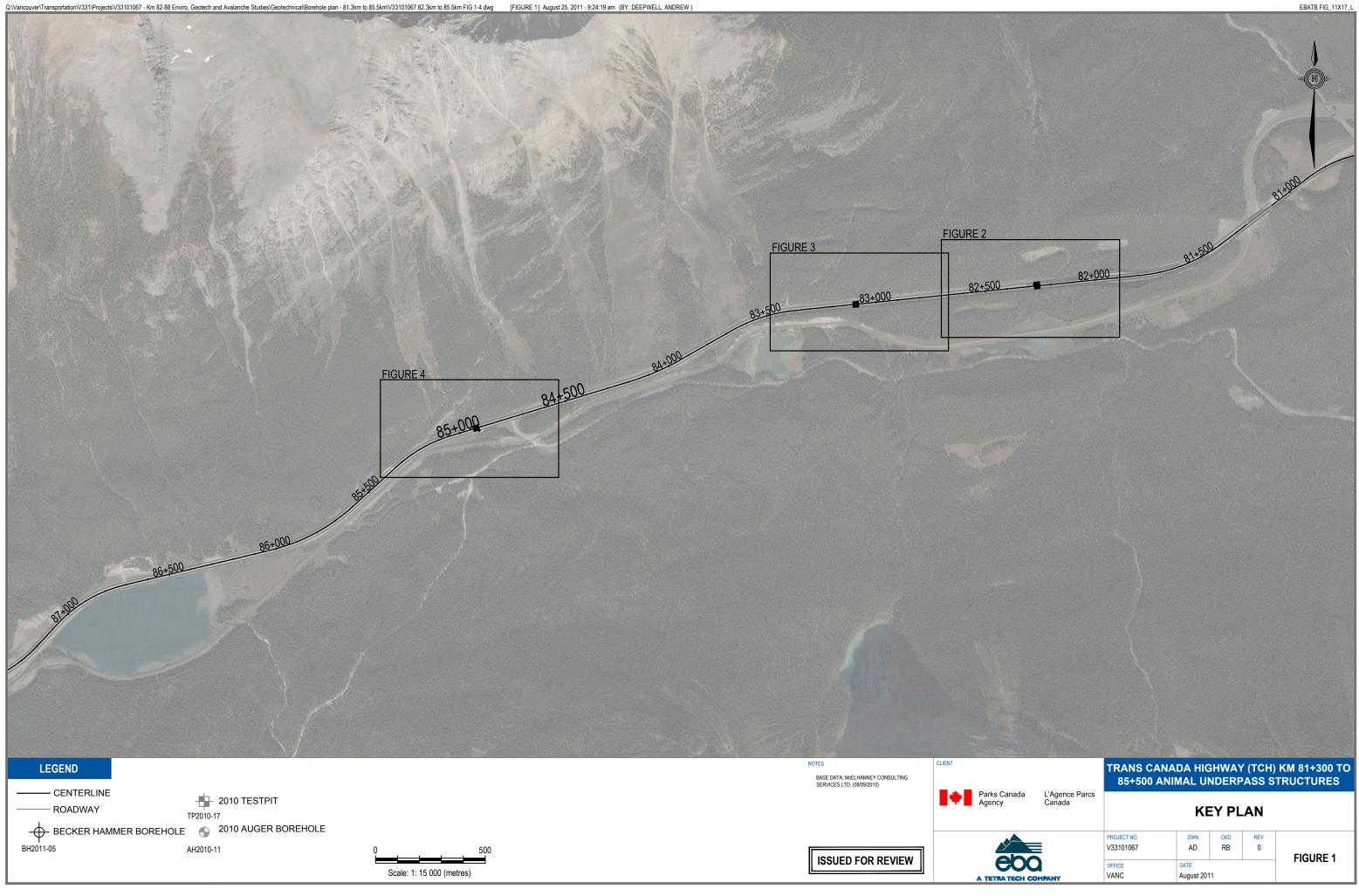
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FIGURES

| Figure I | Key Plan |
|----------|---|
| Figure 2 | Borehole Locations - Underpass at Km 82+260 |
| Figure 3 | Borehole Locations - Bridge at Km 83+090 |
| Figure 4 | Borehole Locations - Underpass at Km 84+920 |



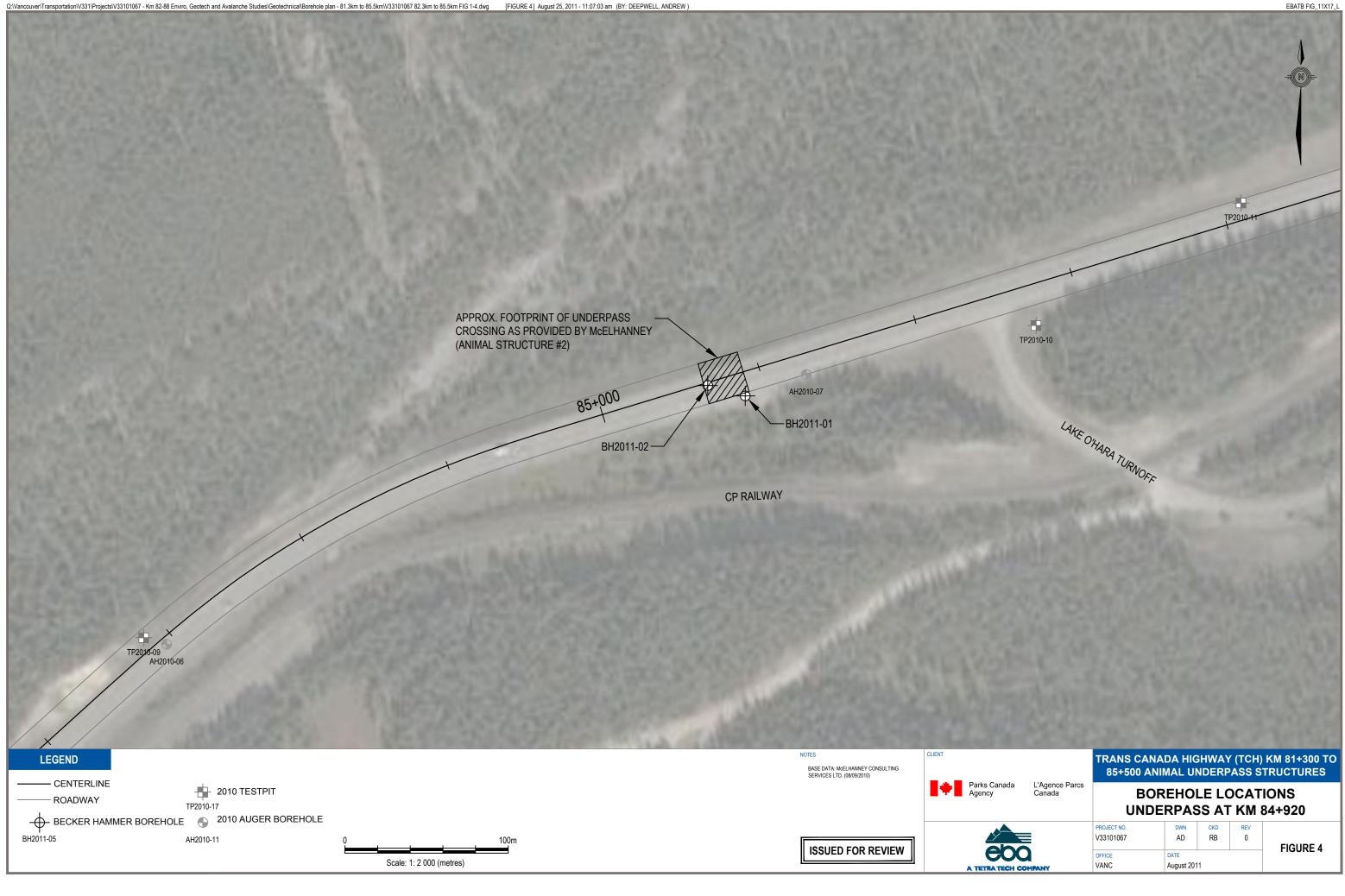


| DWN | CKD | REV | |
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| August 201 | 1 | | |











APPENDIX A APPENDIX A EBA'S GENERAL CONDITIONS

GENERAL CONDITIONS

GEOTECHNICAL REPORT

This report incorporates and is subject to these "General Conditions".

1.0 USE OF REPORT AND OWNERSHIP

This geotechnical report pertains to a specific site, a specific development and a specific scope of work. It is not applicable to any other sites nor should it be relied upon for types of development other than that to which it refers. Any variation from the site or development would necessitate a supplementary geotechnical assessment.

This report and the recommendations contained in it are intended for the sole use of EBA's Client. EBA does not accept any responsibility for the accuracy of any of the data, the analyses or the recommendations contained or referenced in the report when the report is used or relied upon by any party other than EBA's Client unless otherwise authorized in writing by EBA. Any unauthorized use of the report is at the sole risk of the user.

This report is subject to copyright and shall not be reproduced either wholly or in part without the prior, written permission of EBA. Additional copies of the report, if required, may be obtained upon request.

2.0 ALTERNATE REPORT FORMAT

Where EBA submits both electronic file and hard copy versions of reports, drawings and other project-related documents and deliverables (collectively termed EBA's instruments of professional service), only the signed and/or sealed versions shall be considered final and legally binding. The original signed and/or sealed version archived by EBA shall be deemed to be the original for the Project.

Both electronic file and hard copy versions of EBA's instruments of professional service shall not, under any circumstances, no matter who owns or uses them, be altered by any party except EBA. EBA's instruments of professional service will be used only and exactly as submitted by EBA.

Electronic files submitted by EBA have been prepared and submitted using specific software and hardware systems. EBA makes no representation about the compatibility of these files with the Client's current or future software and hardware systems.

3.0 ENVIRONMENTAL AND REGULATORY ISSUES

Unless stipulated in the report, EBA has not been retained to investigate, address or consider and has not investigated, addressed or considered any environmental or regulatory issues associated with development on the subject site.

4.0 NATURE AND EXACTNESS OF SOIL AND ROCK DESCRIPTIONS

Classification and identification of soils and rocks are based upon commonly accepted systems and methods employed in professional geotechnical practice. This report contains descriptions of the systems and methods used. Where deviations from the system or method prevail, they are specifically mentioned.

Classification and identification of geological units are judgmental in nature as to both type and condition. EBA does not warrant conditions represented herein as exact, but infers accuracy only to the extent that is common in practice.

Where subsurface conditions encountered during development are different from those described in this report, qualified geotechnical personnel should revisit the site and review recommendations in light of the actual conditions encountered.

5.0 LOGS OF TESTHOLES

The testhole logs are a compilation of conditions and classification of soils and rocks as obtained from field observations and laboratory testing of selected samples. Soil and rock zones have been interpreted. Change from one geological zone to the other, indicated on the logs as a distinct line, can be, in fact, transitional. The extent of transition is interpretive. Any circumstance which requires precise definition of soil or rock zone transition elevations may require further investigation and review.

6.0 STRATIGRAPHIC AND GEOLOGICAL INFORMATION

The stratigraphic and geological information indicated on drawings contained in this report are inferred from logs of test holes and/or soil/rock exposures. Stratigraphy is known only at the locations of the test hole or exposure. Actual geology and stratigraphy between test holes and/or exposures may vary from that shown on these drawings. Natural variations in geological conditions are inherent and are a function of the historic environment. EBA does not represent the conditions illustrated as exact but recognizes that variations will exist. Where knowledge of more precise locations of geological units is necessary, additional investigation and review may be necessary.

7.0 PROTECTION OF EXPOSED GROUND

Excavation and construction operations expose geological materials to climatic elements (freeze/thaw, wet/dry) and/or mechanical disturbance which can cause severe deterioration. Unless otherwise specifically indicated in this report, the walls and floors of excavations must be protected from the elements, particularly moisture, desiccation, frost action and construction traffic.

8.0 SUPPORT OF ADJACENT GROUND AND STRUCTURES

Unless otherwise specifically advised, support of ground and structures adjacent to the anticipated construction and preservation of adjacent ground and structures from the adverse impact of construction activity is required.

9.0 INFLUENCE OF CONSTRUCTION ACTIVITY

There is a direct correlation between construction activity and structural performance of adjacent buildings and other installations. The influence of all anticipated construction activities should be considered by the contractor, owner, architect and prime engineer in consultation with a geotechnical engineer when the final design and construction techniques are known.

10.0 OBSERVATIONS DURING CONSTRUCTION

Because of the nature of geological deposits, the judgmental nature of geotechnical engineering, as well as the potential of adverse circumstances arising from construction activity, observations during site preparation, excavation and construction should be carried out by a geotechnical engineer. These observations may then serve as the basis for confirmation and/or alteration of geotechnical recommendations or design guidelines presented herein.

11.0 DRAINAGE SYSTEMS

Where temporary or permanent drainage systems are installed within or around a structure, the systems which will be installed must protect the structure from loss of ground due to internal erosion and must be designed so as to assure continued performance of the drains. Specific design detail of such systems should be developed or reviewed by the geotechnical engineer. Unless otherwise specified, it is a condition of this report that effective temporary and permanent drainage systems are required and that they must be considered in relation to project purpose and function.

12.0 BEARING CAPACITY

Design bearing capacities, loads and allowable stresses quoted in this report relate to a specific soil or rock type and condition. Construction activity and environmental circumstances can materially change the condition of soil or rock. The elevation at which a soil or rock type occurs is variable. It is a requirement of this report that structural elements be founded in and/or upon geological materials of the type and in the condition assumed. Sufficient observations should be made by qualified geotechnical personnel during construction to assure that the soil and/or rock conditions assumed in this report in fact exist at the site.

13.0 SAMPLES

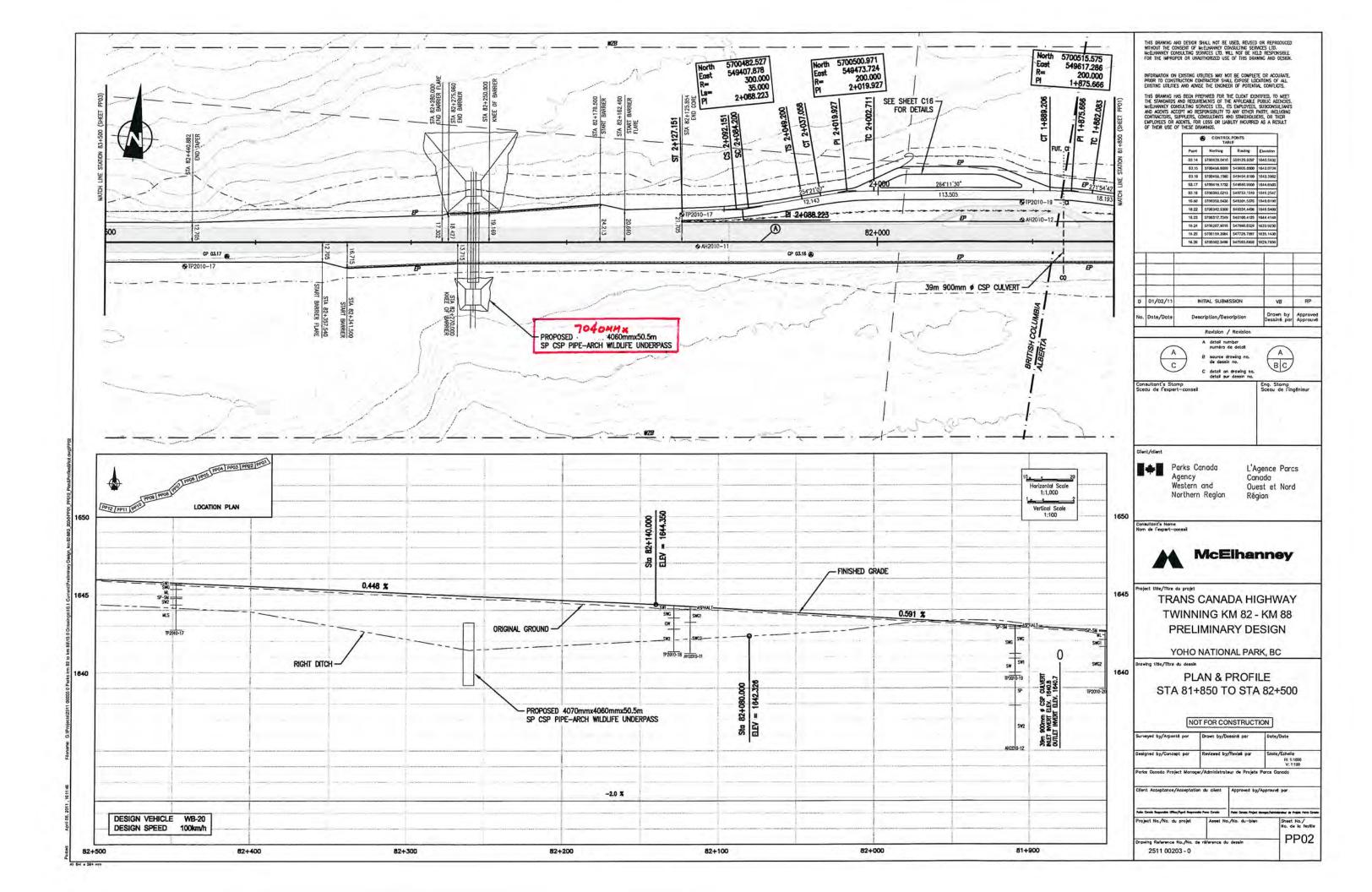
EBA will retain all soil and rock samples for 30 days after this report is issued. Further storage or transfer of samples can be made at the Client's expense upon written request, otherwise samples will be discarded.

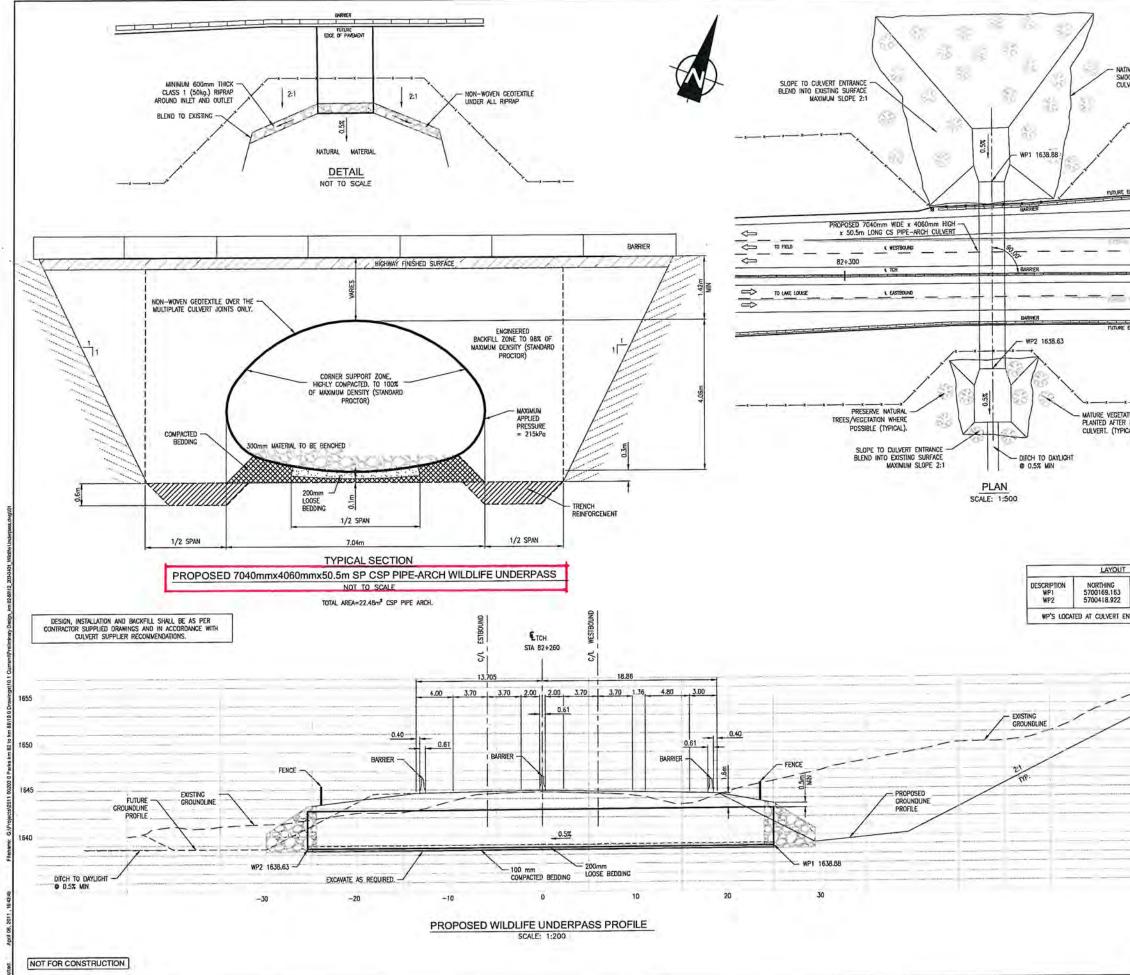
14.0 INFORMATION PROVIDED TO EBA BY OTHERS

During the performance of the work and the preparation of the report, EBA may rely on information provided by persons other than the Client. While EBA endeavours to verify the accuracy of such information when instructed to do so by the Client, EBA accepts no responsibility for the accuracy or the reliability of such information which may affect the report.

APPENDIX B APPENDIX B DRAWINGS PROVIDED BY MCELHANNEY CONSULTING SERVICES

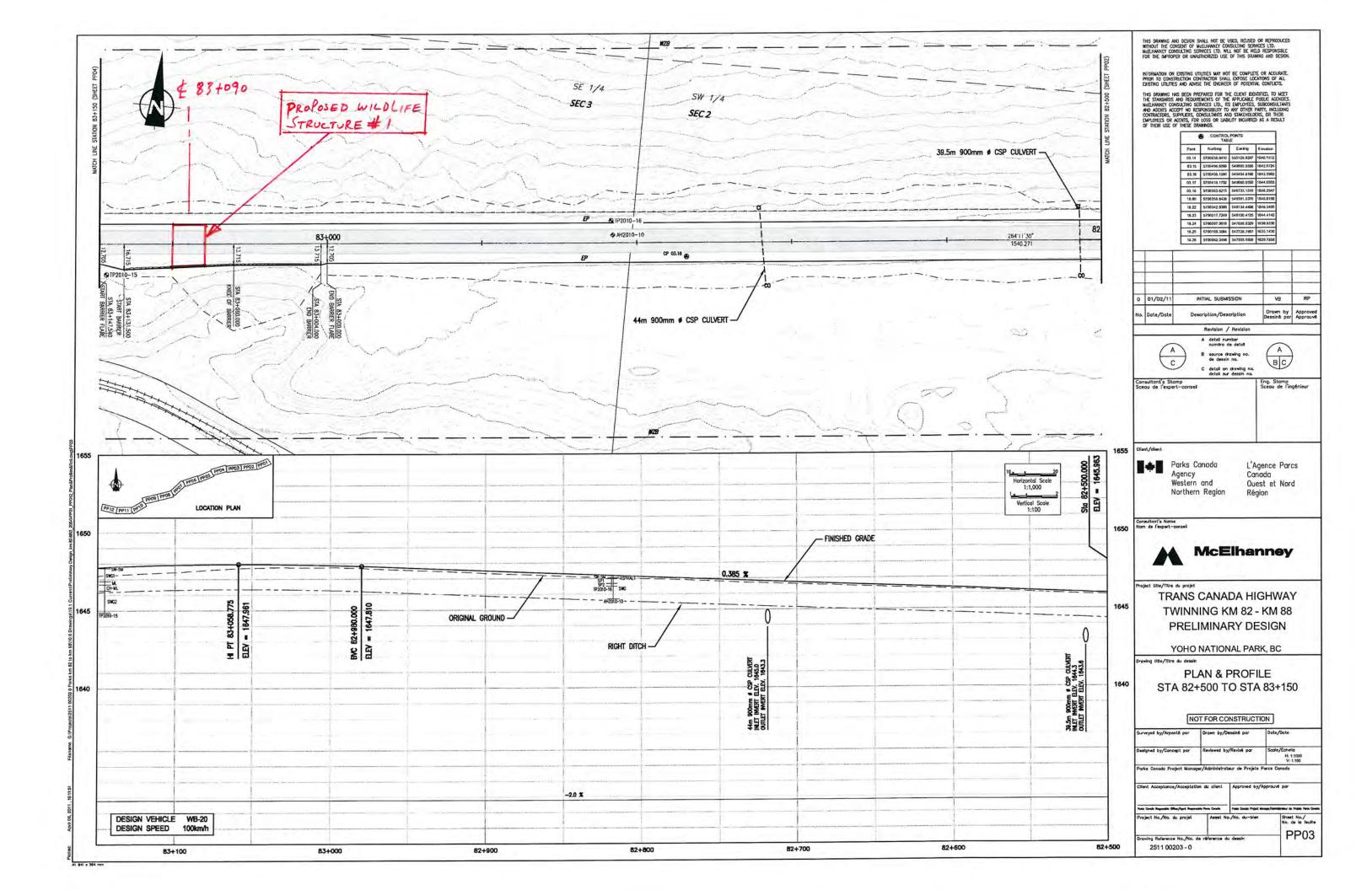


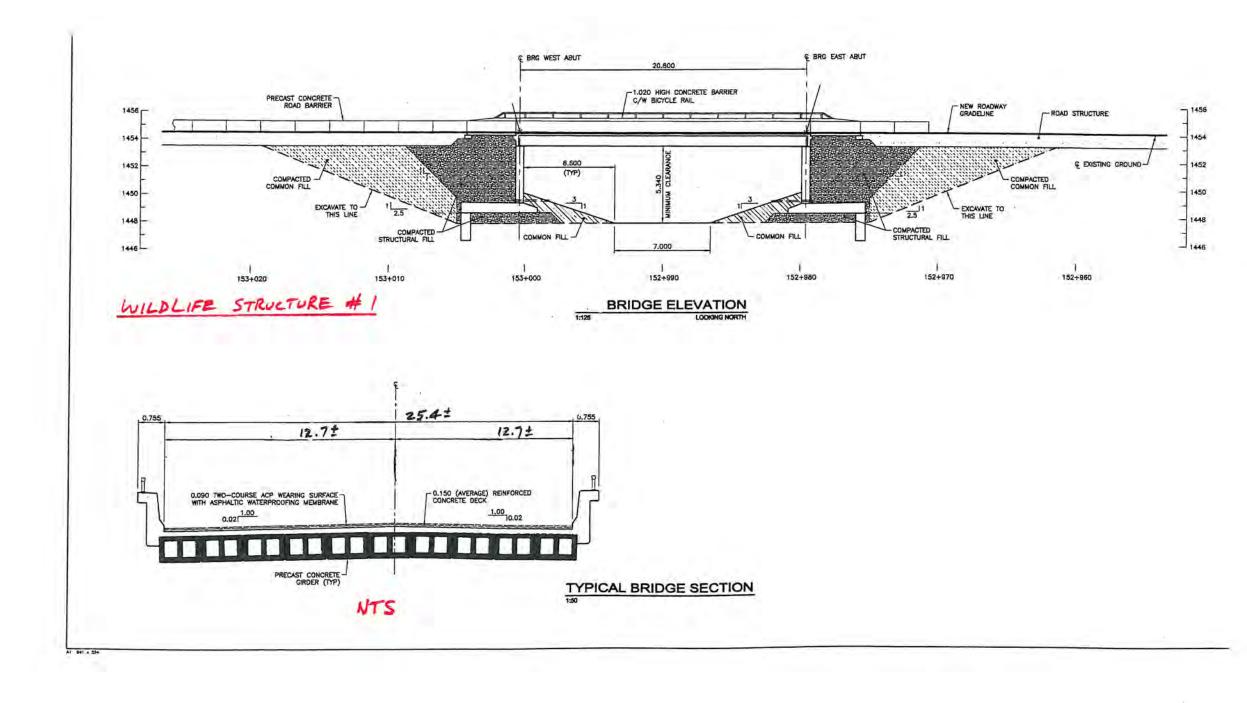




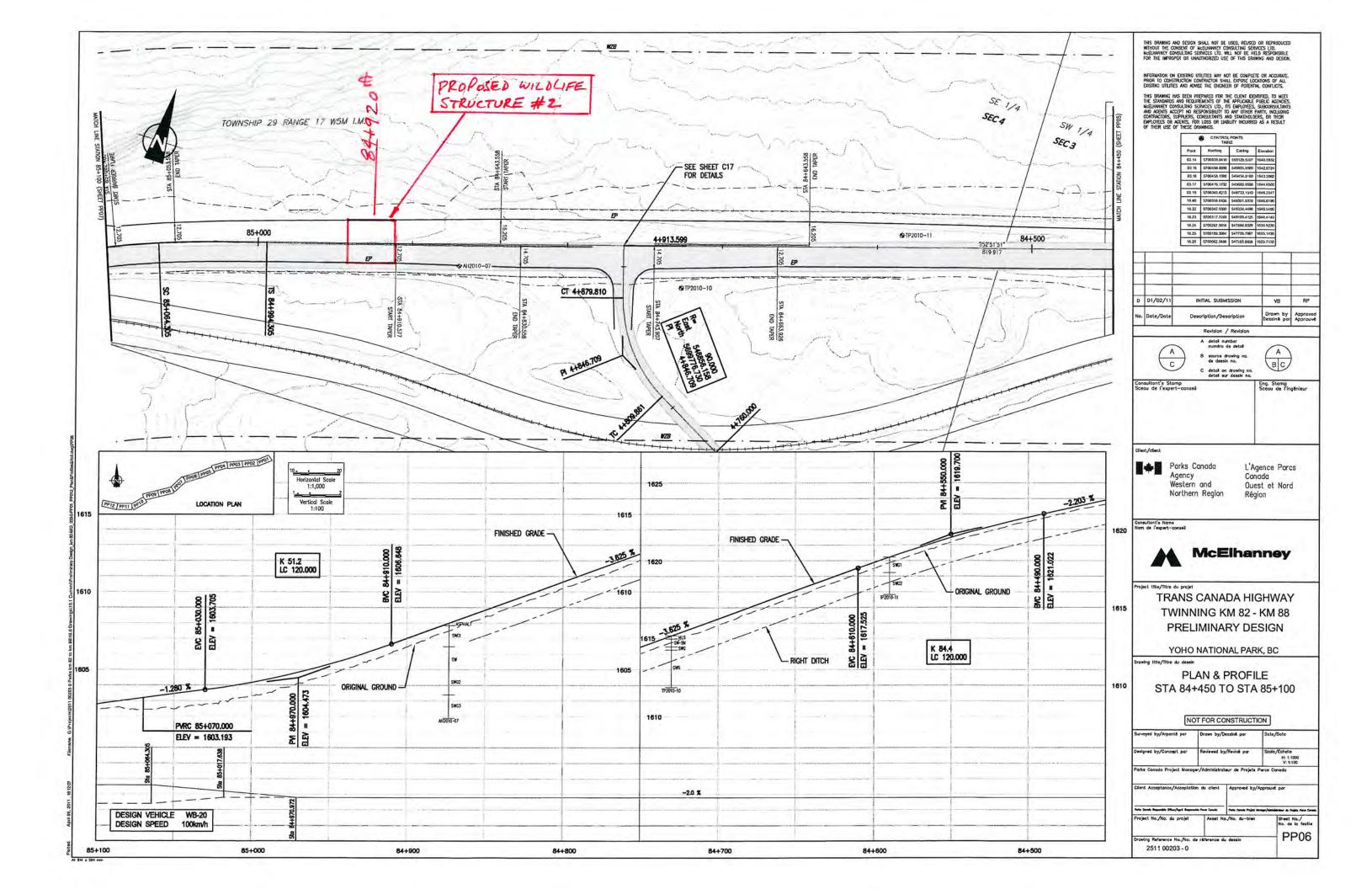
AT 841 x 594 mm

| IVE SOIL MATERIAL PROVIDE JOTH TRANSITION FROM VERT TO EXISTING GROUND. | This drawing and design shall not be used, reused or reproduced infrout the construction welliawing? Consultance Services 10. Weldhammer Consultang Services 10. Will not be fall response to the for the improve or unauthorized use of the drawing and design. Information on existing utilities way not be complete or accurate existing utilities and ansie the Borneer of Potential Contacts. This drawing ins being provide the Drawer of the Control of the accurate the standards of the Drawer of the Control of the existing utilities and ansie the Borneer of Potential Contacts. This drawing ins being symbols of the Accurate Public Acoustings weldhammer to response symbols of the Accurate Public Acoustings weldhammer of response the Control of the Control of the Control weldhammer of the Services of the Control of the Control weldhammer of the Services of the Control of the Control weldhammer of the Services of the Control of the Control weldhammer of the Services of the Services of the Control of the Control weldhammer of the Services of the Services of the Services of the energy of the Services of Lange of the Services of the Services of the Services of the Energy of the Services of the Services of the Services of these energy of the Services of the |
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| EASTING ELEVATION 549225,191 1658.86 549240.302 1658.63 | Client/client Parks Canada L'Agence Parcs Agency Canada Western and Ouest et Nord Northern Region Région Consultant's Name Nom de l'expert-consei |
| DS UNDERSIDE OF CULVERT. | Project title/Titre du projet TRANS CANADA HIGHWAY TWINNING KM 82 - KM 88 PRELIMINARY DESIGN YOHO NATIONAL PARK, BC |
| 1645 | WILDLIFE UNDERPASS PLAN & PROFILE STA 82+260 |
| 1640 | Surveyed by/Anpenté par Drown by/Dessiné par Dele/Dote Designed by/Concept par Reviewed by/Revisé par Scale/Echelle ASSHOWN Parks Canada Project Monoger/Administrateur de Projets Parcs Canada Client Acceptatos/Acceptation de client Approved by/Approved par |
| CONTRACTOR RESPONSELE FOR STRUCTURAL DESIG | Auto Coule Reported Ottor, Part Segmente Pros Project No./No. da projet Asset No./No. da -bien Sheet No./No. No. de la faulte Drawing References No./No. de réferences du dessin 2511 00203 - 0 IO1 |





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APPENDIX C APPENDIX C BOREHOLE LOGS

| Trans | Canada Highway - Km 81.3 to 85.5 | Parks Canada Agency | | | | | | | | | | | P | PROJECT NO BOREHOLE NO. | | | | | | |
|-----------|---|---------------------|---------------|-----------------------|--------|------------|-------------------|----------|------|---------|------------------|------|------------------------|--|-----------|-------|------------|--|--|--|
| South | Side of Highway | B | Becker Hammer | | | | | | | | | | | V33101067 BH2011-01 | | | | | | |
| N. 569 | 9786.3 E. 546700.7 | | | | | | | | | | | | ELEVATION: 1606m | | | | | | | |
| SAMP | LE TYPE 🔄 DISTURBED 🛛 NO RECOV | 'ERY | ′ D | SPT | | | | -CASI | NG | | SHELBY TUBE CORE | | | | | | | | | |
| BACK | FILL TYPE BENTONITE 🚺 PEA GRAV | EL | Π | SLO | UGH | | GROUT DRILL | | | | | | | TTING | s 🗄 | : 5 | AND |) | | |
| | | ш | ER | | | | Ę | | | | | | | | | | | | | |
| Ê | | TYPE | SAMPLE NUMBER | ~ | | SYMBOL | VIOISTURE CONTENT | <u> </u> | | | | | BECKER PENETRATION (N) | | | | | E E | | |
| th (r | OOIL | ш | NN | BPT (N _b) | USC | MΥ | 8 | | | | | | | . · | 40 | 80 | 1: | 20 | 160 | tion |
| Depth (m) | DESCRIPTION | SAMPL | Ц | BP | | <u>⊣</u> | IJURI | PLA | STIC | м | С | LIQU | ЛD | | •UN 50 | | | D (kP 50 | | Elevation (m) |
| | | SA | AMI | | | SOIL | NOIS NOIS | ' | - | | • | | | | | CKET | I PEN | N. (kP | °a) 🔺 | |
| - 0 | ASPHALT (150 mm) | | S | 33 | ASPHAL | | | | 20 | 40 | 6(|) 8 | | | 00 | 200 |) 31 | 00 | 400 | 1606.0 |
| E | GRAVEL and SAND, some silt, occasional cobbles, | | | | | | | | | | | | | | | | | | | - |
| - | fine gravel, medium to coarse sand, sub-angular to sub-rounded, damp, compact, | | 1 | 34 | | | 4.8 | | | | ·[···] | | | | E | | | | ··÷··† | |
| Ē, I | tan. | | 1 | 25 | SWG | ຳ. ເຜີຍ | 4.0 | | - | | | | | | | | | | | 1005.0 |
| | | | | 26 | | а. С | | | Ť | | | | | - in in in it is a state of the | ÷ | i i | | | - | 1605.0 |
| Ē | | | | 36 | | f | | | | | | | | | | | | | | |
| - | SAND, some silt, some gravel, fine to medium sand, | | | 56 | | Ì | | : | | ···· | 1 | | | | | ••••• | | l de la composición de la comp | ··•••••• | |
| E , I | well graded gravel, sub-angular, damp, very dense, tan. | | 0 | | | | | | | | | | | | 1 | | | | | 1004.0 |
| 2 | uchilo, tan. | \vdash | 2 | 169 | | | 4 | | Ť | | 11 | | | | ÷ | t t | | int i | | 1604.0 |
| Ē | -possible boulder at 2.6 m depth | | | 232 | | | | | | | | | | | | | | | | 237 - |
| - | SAND, some silt, some gravel, occasional cobbles, | | | 337 | | | | | | | | | | | 1 | | | | | |
| E 3 | fine to medium sand, well graded gravel, | | | 295 | | | | | | | | | | | | | | | | ²⁹⁵ |
| E | angular, damp, dense to very dense, tan, trace wood debris. | | | 146 | | | | | Ì | | | | | | 1 | i i | 1 | | | |
| - | | | | 140 | | | | | | | | | | | | | | 1 | | = |
| E | | | | 86 | | | | | | | | | | | 1 | • | r; | | | |
| - 4 | | | | 75 | | | | | | | | | | | | | | | | 1602.0 |
| | | F | 3 | 88 | | | 3 | • | | | | | | | 1 | | | | | |
| F | | | | 56 | SP-SM | | | | | | | | | | | | | | | - |
| Ē | | | | 52 | | | | | Ĩ | | | | | | | | T | | Ī | |
| 5 | | | | | | | | | | | | | | | - | | | | | |
| - | | | | 52 | | | | | | | | | | | | | | | | = |
| E | | | | 73 | | | | | | ļ | | | | | Į | | | | | |
| F | | | | 73 | | | | | | | | | | | | | | | | - |
| E 6 | | | | 50 | | | | | | | | | | | | | | | | 1600.0 |
| F | -frequent fractured pieces of rock at 6.1 m depth | | | 39 | | | | | | | | | | | | | | | | |
| E I | (likely broken up cobbles or boulders) | | | 38 | | | | ļļ | Ļ | ļļ | .ii | | | ļ | <u>]</u> | ļļ. | | ļ | | |
| È | | | | | | | | | | | | | | | | | | Li | | - |
| <u> </u> | CAND menually three silt or and sould well mended | | | 124 | | ų | | | | ļļ | | | | | ļ | ļļ. | | | | 1599.0 |
| | SAND, gravelly, trace silt, coarse sand, well graded gravel, sub-rounded to sub-angular, damp to | | | 80 | | ¢. , | | | | | | | | | | • | | | | - |
| - | moist, loose to dense, speckled tan, black and white. | | | 24 | |). | | . | | ļļ | | | | | ļ | ļļ. | | | | |
| Ē | -the drill rods sank with almost no effort in this | \square | 4 | 13 | SPG | 0. | 6 | • | | | | | | | | | | | | - |
| - 8 | material | | | 59 | | ٥. | | | · | | · | | | | ÷ | | | | | 1598.0 |
| - | ODAUEL and the feat and the distance | | | 134 | | •[| | | | | | | | | | | | | | = |
| - | GRAVEL, sandy, fine gravel, medium to coarse sand, sub-rounded to sub-angular, damp to | | | | | | | - | | | · | | | | ÷ | | - <u>-</u> | | | |
| F | moist, very dense, speckled tan, black and white. | | | 100 | GWS | | | | | | | | | | | | | | | - |
| - 9 | | | | 70 | | | | ! | ÷ | | · | | | ! | ÷ | | | ŀ | | 1597.0 |
| E | GRAVEL and SAND, silty, fine to medium sand, fine gravel, sub-rounded to sub-angular, damp to | | | 60 | | | | | | | | | | | 1 | | | | | = |
| F | moist, dense to very dense, tan. | \square | 5 | 68 | | | 6.9 | | ÷ | | · | | | | ÷ | | | | ··•••••••••••••••••••••••••••••••••••• | |
| E 10 | | | | 70 | | | | | - | Í | | | | | | | | | | |
| 10 | | | | /6 | | 6: 47: | OGGE | D B | Y: R | : RB | | | | CON | MPL | ETI | ON | DEP | • • • •TH: • | <u> 1596.0 </u> |
| Ê | 🖥 EBA, A Tetra Tech Co | F | EVIE | NED | ΒY | | | | | | | | | 13/2 | | | | | | |
| | | | RAW | NG I | NO: | | | | | Pag | | | | | | | | | | |

| | Trans Canada Highway - Km 81.3 to 85.5 | | | | | | Parks Canada Agency | | | | | | | | | | PROJECT NO BOREHOLE NO. | | | | | | | | | | |
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| | Side of High | | | Be | ecker | r Hamr | ner | | | | | | | | V33101067 BH2011-01 | | | | | | | | | | | | |
| | 99786.3 E. 5 | 46700.7 | | | | _ | | | | | | | | _ | ELEVATION: 1606m | | | | | | | | | | | | |
| | PLE TYPE | | NO RECOV | | | SPT | | | | | | | | | | LBY TUBE CORE | | | | | | | | | | | |
| BACK | FILL TYPE | BENTONITE | PEA GRAV | EL | Щ | SLO | UGH | | <u> </u> | ROU | Т | | \sim | DRILI | _ CU1 | TTIN(| GS [| ° ° ° | SAN | D | | | | | | | |
| | | | | TYPE | SAMPLE NUMBER | | | Ы | MOISTURE CONTENT | | | | | | | | | | | | | | Ê | | | | |
| E) | | SOIL | | ≽ | MU | (N ^b) | U | SYMBOL | | | | | | | | BECKER PENE 40 80 | | | | IETRATION (Ŋ) ■ 120 160 | | | u (n | | | | |
| Depth (m) | | DESCRIPTIC | ΟN | Ш | щ | BPT (N _b) | USC | ∑ | ۱ ۳ | | | | | | | • | ♦ UN | NCON | NFINE | ED (kl | Pa) 🔶 | | Elevation (m) | | | | |
| | | | | SAMPL | MP | | | SOIL | DIST | PLA | STIC | ; N | I.C. ● | | ID | | 50 ▲PC | | | | 200 Pa) ▲ | _ | Ele | | | | |
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| Ē ' | -coarsening | | | 96 | | | | | | | | | | | | | | | | | - | | | | | | |
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| E 12 | | | | | | | | | | | | | | | | | | | | | | | 1594.0 | | | | |
| E | SAND trace | gravel, trace silt, coarse | sand fine | | | 50 | | | | | | | | | | | | | | | | | - | | | | |
| - | grave | , sub-rounded, damp to r | noist, dense to | | 6 | 55 | | | 11 | | | | | | | | | | | | | | _ | | | | |
| Ę | | ense, speckled black and nd silt material intermixed | | | Ů | 80 | | | | | | | | | | | | | | | | | - | | | | |
| 13 | i mater | al e silt, trace clay, trace gra | | | | 94 | | | | | | | | | | | | | | | | ···· | 1593.0 | | | | |
| | mediu | m sand, fine gravel, sub- | rounded, damp | | | 86 | | | | | | | | | | | | | | | | | - | | | | |
| | to moi | st, very dense, low plasti | c, tan. | | | 192 | SP | | | | 1 | | | | 1 | | 1 | | | | | | - | | | | |
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| Trans | Canada Highway - k | nada A | gency | | | | PROJECT NO BOREHOLE NO. | | | | | | | | | | | | |
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| North | Side of Highway | | | Beck | er Ha | ammer | | | | | | V33101067 BH2011-02 | | | | | | | |
| N. 569 | 99792.7 E. 546677.7 | | | | | | | | | | | ELEVATION: 1605.4m | | | | | | | |
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| BACK | (FILL TYPE 🔄 BEN | NTONITE | PEA GRAVE | L [| | SLOUGH | | | GROUT | | DRILI | . CUT | TINGS | S 👬 | SAN | D | | | |
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| - 0 | ASPHALT (150 mm) | | | ASP | HAL | ્ | | | | | | | | | | - | | | |
| Ē | | d gravel, sub-ro | unded to sub-angu | ılar, | | | | î | | | | | | | | | | 1605.0 | |
| F | damp, tan, conta | ains broken piec | es of rock. | | | | ÷. | • | | | | | | | | | | = | |
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| - | | h trace clay. e recovery from 12.2 to 1 | 12.1 m | | | SP | · | | | | | | | | | | | | | | 1593.0 | | |
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| E 13 | SILT and Si | AND (TILL-like), trace cla n rock, fine sand, moist, t | y, occasional piece | s of | | 5 | | 13 13 | | | | | | | | Į | | | | | | | |
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| Ē | tan wi | th grey pieces of rock. | of broken rock, mo | | | | | | | | | | | | | | | | | | | | |
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| - 0 | SAND, grave | elly, trace silt, well grade | d sand, fine | + | Ś | | | å | 2 | <u>+</u> : | 20 | 4 | 0 | 60 | 80 | | 10 | 10 2 | 200 | 300 | 400 | : | _ | |
| E | gravel | , sub-rounded, damp, br | own, occasional | | | | SWG | . 8. •] | | | | | | | | | | | | | | | 1647.0 | |
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| Ê. | SAND and C broker | RAVEL, some silt, occa rock, well graded sand | sional pieces of and gravel, | | | | | | | | | | | | | | | | | | | | - | |
| 1 - | angula | angular to sub-rounded, damp. | | | | | | | | | ···• | 1 | | | | | 11 | | 1 | | 1 | ÷ | - | |
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| E 3 | | RAVEL, trace silt, occas | | | | | | |] | | | | | | | | | | | | | | - | |
| - 3 | | broken rock, well graded sand and gravel, sub-rounded to sub-angular, damp, brown. | | | | | | | | | ···• | 11 | | | | | 11 | | 1 | | | 1 | = | |
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| Ē | SAND grave | elly, trace silt, medium to | coarse sand | ∇ | 2 | 15 | | | 2.7 | | | | | | | | | | 1 | | | | - | |
| L 5 | fine gr | avel, sub-angular, damp | to moist, | \square | | 10 | | | | | | | | | | | | | | | | | _ | |
| - | | act, speckled brown, blac 5 to 5.1 m (8-8-7-8) | k and grey. | | | | | <u>}</u> | | | | | | | | | | | 1 | | | | 16420 - | |
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| - | SAND, grave | elly, trace silt, occasional | cobbles, well | | | 47 | | | | | 1 | | | | | | | | • | | 11 | 1 | _ 1641.0_ | |
| Ē | | d sand and gravel, sub-rongular, damp, dense, bro | | | | | | · | | | | | | | | | | | | | | | | |
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| E 9 | -gravel beco | ming angular to sub-ang | jular at 8.8 m | | | | | | | | | | | | | ļ | | | .ļ | ļļ | .įį. | | | |
| È | | 10 m poor recovery of br | oken pieces of | F | 5 | | GWS | | 3 | • | | | | | | | | | | | | | - 1638.0 | |
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| Trans | Canada Hig | hway - Km 81.3 to 85 | .5 | F | Parks (| Canada | a Agei | ncy | | | | | | | P | ROJ | ECT | NO |) B | ORE | HOL | E NO. |
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| North | Side of High | way | | E | Becker | Hamn | ner | | | | | | | | | V3 | 310 | 106 | 7 | BH2 | 011-0 |)4 |
| N. 570 | 00370.0 E. 5 | 48419.1 | | | | | | | | | | | | | EL | EVAT | 101 | I: 16 | 647.3 | m | | |
| SAMF | PLE TYPE | DISTURBED | NO RECO | OVER | XY 🛛 |] SPT | | | | -CAS | ING | | | _ | | UBE | | | ORE | | | |
| BACK | FILL TYPE | BENTONITE | PEA GRA | | | SLOU | JGH | | • | ROU | Γ | | \square | DRIL | L CU | TTING | s 🗄 | °, S | AND | | | |
| | | | ш | SAMPLE NUMBER | | | | Ľ | IN I | | | | | | | | | | | | | _ |
| Ê | | SOIL | TYPE | ۳ | 7 | Î | \sim | SYMBOL | MOISTURE CONTENT | | | | | | | | | | | TION | | Elevation (m) |
| Depth (m) | г | | Щ | Ξl | BPT (N _b) | SPT (N) | usc | SYN | l ů | <u> </u> | | | | | | | 40 - UNC | 80 CONF | 12 INED | 0 16 (kPa) | | atior |
| Del | L | DESCRIPTION | SAMPLE | 11 | 8 | R | | SOIL | STUP | PLA | STIC | M. | .C. | LIQU | ЛD | 1 | 50 | 100 | 15 | 0 20 | 00 | leve |
| | | | SP | SAN | | | | S(| ₩ W | | 20 | 40 | 6(| |) | | .POC 00 | KET 200 | | . (kPa) 0 40 | | Ш |
| - 0 | ASPHALT (| | | | 27 | į | ASPHAI | (. | | | 1 | Ĩ | TÌ | | | | Î | | T | | | |
| F | SAND, grav and o | elly, trace silt, well graded ravel, sub-rounded to | sand | | 19 | | | 0°°° | | | | | | | | | | | | | | 1647.0 |
| E | sub-a | ngular, damp, loose to cor | npact, | | 17 | | | <u>.</u> | | | | | | | | | Ī | Ĩ | | | | - |
| Ē1 | brown | l. | | | | | | °°°° | | | | | | | | | | | | | | |
| F | | | | | 20 | | | <i>2</i> .,, | 1 | | | | | | | | | | | | | - 1646.0 |
| E | | | | | 24 | | | .•.•.).•.• | | | | | .j; | | | | į | | ļ | | ļ | |
| E | | | | | 14 | | | ŝ | | | | | | | | | | | | | | - |
| _ 2 | | | | | 11 | | SWG | °., | | | | | | | | | ļļ | | | | ļ | |
| E | | | | | 10 | | 5WG | | | | | | | | | | | | | | | - 1645.0 |
| F | | | | | 11 | | | .°°° | | ! | 4 | | | | | . | . | | | | ļ | |
| E | | | | | 9 | | | ç.,, | | | | | | | | | | | | | | _ |
| - 3 | | | | | | | | (| | | · • • • • | | · | | | | | | $\left\ \cdot \right\ $ | | | - |
| F | | | | | 11 | | | ૾૾ૺ૾૾ | | | | | | | | | | | | | | 1644.0_ |
| - | | | | | 11 | | | ÷ | } | | ·†··· | | ·[···] | | | . | | | + | | | |
| Ê, | | | | | 14 | | | | | | | | | | | | | | | | | - |
| F 4 | | e gravel, medium to coars | | | 19 | | | <u>}</u> | | | · • · · • | ···· | 1 | ···• | · | | ÷··· | ···;·· | ÷ | | | = |
| E | | fine gravel, sub-rounded t ngular, compact, speckled | | 1 | 19 | | SPG | o. (| 3 | • | | | | | | | | | | | | 1643.0 |
| E | and b | | | | | | arg | 0 | | | Ť | 1 | | | 1 | | ŤŤ | 1 | ŤŤ | | | 1 - |
| L 5 | CAND trees | e gravel, trace silt, occasio | nal | | 22 | | | <u> </u> | | | | | | | | | | | | | | - |
| Ē | cobble | es, medium to coarse sand | d, fine | 2 | 28 | 20 | | | 2.5 | • | | | | | | | 11 | 1 | | | | 1642.0 |
| Ē | | l, sub-angular to sub-roun , compact, brown. | ded, | | 33 | | | | | | | | | į | | | ļ. | | | | ļ | |
| F | | to 5.6 m (6-8-12-12) | | | 34 | | 0.0 | | | | | | | | | | E | | | | | = |
| E 6 | | | E | 3 | 23 | | SP | | 2 | • | | | | | | | | | | | | |
| E | | | | | 18 | | | | | | | | | | | | | | | | | - 1641.0 |
| E | | | | | 21 | | | | | | | | .i | | | | Ļ., | | ļļ | | ļ | |
| Ē | SAND. grav | elly, some silt, well graded | sand. | | | | | °.° | | | | | | | | | | | | | | - |
| <u> </u> | fine g | ravel, sub-angular to | | | 23 | | | | | | | | · | | | | <u>.</u> | | | | ļļ | |
| F | dense | ounded, damp, compact to e, brown, occasional piece | | | 34 | | | ÷ | | | | | | | | • | | | | | | 1640.0 |
| - | brown | silty clay. | | | 40 | | SWG | ŝ | = ^ | | | | | | | ļļ | | | + | | | - |
| È. | | | H | 4 | 29 | | | °°°f | 5.9 | | | | | | | • | | | | | | - |
| - 8 | | | | | 21 | | | | | | • | | · | | | . | ÷; | | ÷ | | | - |
| Ē | | dense at 8.1 m at 8.3 m - Refusal (possib | | | 15 | | | ° | - | | | | | | | | | | | | | 1639.0 |
| - | bedro | | | | 7 | | | | | | ÷ | | - | | | | ÷ | | ÷ | | | - |
| Ē | | | | | · | | | | | | | | | | | | | | | | | - |
| E 9 | | | | | 50 | | | | | | | | | | | | | | | | | - |
| F | | | | | 46 | | | | | | | | | | | | • | | | | | 1638.0 |
| Ē | | | | | 144 | | | | | | Ì | | | | | | ÎÎ | Î | | • | Ĩ | = |
| - 10 | | | | | 500 | | | | | | | | | | | | | | | | 500 | - |
| ERA A Tatra Taah Ca | | | | | | | | | OGG | | | | | | | | | | | | H: 10 | .1m |
| Ê | at EBA, A Tetra Tech Co | | | | | ТУ | | | REVIE | | | ΚW | | | | CON Page | | | : 6/1 | 5/201 | 11 | |
| GEOTECH | NICAL V33101067 BC | | | | | | NG | ٩Ū. | | | | | rage | 510 | лΖ | | | | | | | |

| Trans Canada Highway - Km 81.3 to 85.5 North Side of Highway | | | | | Parks Canada Agency PROJECT NO BOREHC Becker Hammer V33101067 BH2011 | | | | | | | | | | | | | | | | | | |
|---|---|--|-------------|---------------|--|---------|-----|-------------|------------------|-------|-------|------|--------|----------|-------|------|------------------|-----------------|-----------------|----------------------------|--------------|-----------|----------------------------|
| | | | | | Becker | Hamm | er | | | | | | | | | | | | | | | 1-04 | 1 |
| | 00370.0 E. 5 | | _ | | | 2 | | | | | | | | | | | - | _ | | 7.3m | | | |
| | PLE TYPE | | NO RE | | ~ | SPT | | | | -CASI | | | Щ | SHEL | | | | | COF | | | | |
| BACK | FILL TYPE | BENTONITE | PEA C | | ĻЩ | SLOU | GH | | <u> </u> | ROUT | | | \geq | DRILL | . CUT | TING | GS [| | SAN | D | | _ | |
| Depth (m) | C | SOIL DESCRIPTION | SAMPLE TVDE | SAMPLE NUMBER | BPT (N _b) | SPT (N) | NSC | SOIL SYMBOL | MOISTURE CONTENT | PLAS | STIC | M | .C. | LIQUI | D | • | 40 ♦ UN 50 | 8 NCOI 10 | 0 NFIN)0 | <u>120</u> ED (k 150 | | | Elevation (m) |
| | | | 10 | SAN | | | | S(| Ň | | 20 | 40 | 60 | 80 | | | ▲PC 100 | | et pe)0 | EN. (k 300 | Pa) ▲ 400 | | ш |
| - 10 | EOH (closed | d) at 10.1 m | | | | | | | | | | | | | | | | | | | | 1 | 1637.0_ |
| - - - - - - - - - - - - - - - - - - - | -the closed botton | Becker hole had water at n at 9.8 m depth | the | | | | | | | | | | | | | | | | | | | | - |
| 12 | | | | | | | | | | | ¢, | | | | | | | | | | | 1 | 1636.0 |
| | | | | | | | | | | | | | | | | | | | | | | 1 | 1635.0 |
| 13 | | | | | | | | | | | | | | | | | | | | | | 1 | - 1634.0 - - |
| 14 | | | | | | | | | | | ¢ | | | | | | | | | | | 1 | |
| 15 | | | | | | | | | | | ····· | | | | | | | | | | | 1 | 1632.0 |
| 16 | | | | | | | | | | | | | | | | | | | | | | 1 | |
| - - 17 | | | | | | | | | | | ····· | | | | | | | | | | | 1 | - - - 1630.0 - |
| 18 | | | | | | | | | | | | | | | | | | | | | | 1 | 1629.0_ |
| 19 | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | ÷ | | | | | | | | | | | | 1628.0 |
| | | A Totro T | och (| <u></u> | nno | 201 | | | | | | | | | | 00 | MP | LET | ION | I DE | PTH: | 10. | 1m |
| Ê | | , A Tetra T | ecn (| JOI | npai | чy | | | | | | ΚW | | | _ | | | LE I ? of 2 | | 6/15/2 | 2011 | | |
| GEOTECH | TECHNICAL V33101067 BOREHOLE LOGS (AUGUST 25, 2011) GPJ EBA GDT 8/25/11 | | | | | | | | | | гa | je 2 | . 01 4 | <u> </u> | | | | | | | | | |

| Trans Canada Highway - Km 81.3 to 85.5 | Parks Canada Agency PROJECT NO BOREHOLE Becker Hammer V33101067 BH2011-05 | | | | | | | | | |
|--|---|---|-------------|------------------|--------------------|--|--|--|--|--|
| North Side of Highway | Becke | r Hammer | | | | V33101067 BH2011-05 | | | | |
| N. 5700451.3 E. 549224.0 | | _ | | | | ELEVATION: 1644.5m | | | | |
| SAMPLE TYPE DISTURBED NO RECOV | | SPT | | | | BY TUBE CORE | | | | |
| BACKFILL TYPE BENTONITE PEA GRAVE | | SLOUGH | 1 | <u> </u> | GROUT 🛛 DRILL | . CUTTINGS 🔃 SAND | | | | |
| | SAMPLE TYPE SAMPLE NUMBER | BPT (N _b) | SOIL SYMBOL | MOISTURE CONTENT | PLASTIC M.C. LIQUI | ■BECKER PENETRATION (N,) ● 40 80 120 160 ● UNCONFINED (kPa) ◆ 50 100 150 200 ▲ POCKET PEN. (kPa) ▲ 100 200 300 400 | | | | |
| O ASPHALT (160 mm) GRAVEL and SAND, trace silt, occasional cobbles, | | 46 ASF | PHAL | | | | | | | |
| frequent pieces of broken rock, well graded sand and gravel, angular to sub-rounded, damp, dense, brown with white pieces of rock. SAND, gravelly, trace silt, occasional cobbles, occasional pieces of broken rock, well graded sand and gravel, sub-angular to sub-rounded, moist, compact to dense, reddish brown sand with grey pieces of rock. 2 3 GRAVEL and SAND, trace silt, occasional cobbles, medium to coarse sand, fine gravel, angular to sub-angular, wet, compact to dense, brown sand with black and grey gravel. 3 GRAVEL, sandy, trace silt, occasional cobbles, medium to coarse sand, well graded gravel, angular to sub-angular, wet, ormpact to dense, brown sand with black and grey gravel. 4 GRAVEL, sandy, trace silt, occasional cobbles, medium to coarse sand, well graded gravel, angular to sub-angular, very wet, very dense, brown with black and grey gravel. 5 6 | 1 2 3 | 79 70 68 55 40 29 29 29 29 29 55 6 55 | sws | 6 | | 1644.0 | | | | |
| | | | | | | 1637.0 | | | | |
| | | | | | ED BY: RB | COMPLETION DEPTH: 3.9m | | | | |
| 🗦 🚓 EBA, A Tetra Tech Co | тра | ny | | | WED BY: KW | COMPLETE: 6/15/2011 | | | | |
| GEOTECHNICAL V33101067 BOREHOLE LOGS (AUGUST 25, 2011). GPJ EBA GDT 8/25/11 | | | | JRAW | ING NO: | Page 1 of 1 | | | | |

| Trans | Trans Canada Highway - Km 81.3 to 85.5 South Side of Highway | | | | | Parks Canada Agency PROJECT NO BOREHOLE NO. Becker Hammer V33101067 BH2011-06 | | | | | | | | | | E NO. | | | | | | |
|-----------|---|---|-----------------------|----------|---------------|---|------|--------------------|------------------|------|----------|--------|------|------|-------|-------|-------------|-------------|-------------|-----------------|-------|--------------------------|
| | N. 5700437.7 E. 549246.3 | | | | ecker | r Hamr | ner | | | | | | | | | | | | | | 011-0 | 6 |
| | | | _ | | | | | | | | | | | | | EVA | | _ | | m | | |
| | | | | | | SPT | | | | -CAS | | | | _ | LBY 1 | | | | ORE | | | |
| BACK | FILL TYPE | BENTONITE | PEA GRAV | EL | | SLOI | JGH | | <u> </u> | ROU | IT | | | DRIL | LCU | TTING | is ្រុំ | ំូន | and | | | |
| | | | | Ш | BE | | | 5 | ET | | | | | | | | | | | | | Ē |
| (m) | | SOIL | | TYPE | ΜN | (^q N | O | SYMBOL | | | | | | | | ■BE | ECKEF 40 | R PEI 80 | NETR/ 12 | | | u |
| Depth (m) | | DESCRIPTIO | N | PLE | ZЦ | BPT (N _b) | USC | γ | 문 | | | | | | | | | | INED | (kPa) | • | Elevation (m) |
| ð | | DECORA HO | | SAMPL | SAMPLE NUMBER | В | | SOIL | MOISTURE CONTENT | PLA | |) N | 1.C. | | JID | | 50 POC | 100 KET | | 0 20 . (kPa) | | Ele |
| | | | | S | SA | | | | <u>₹</u> | ļ, | 20 | 40 | 6 | 0 8 | 0 | | 100 | 200 | | | | |
| - 0 | | elly, trace silt, well graded I, sub-angular to sub-roun | | | | 8 | SWG | ¢.`` | | | | | | | | | | | | | | |
| - | comp | act, greyish brown. | | \vdash | 1 | 20 | 0110 | 200 | 3 | • | | ļļ. | | | | | . . | | | | | 1644.0 |
| E | SAND and | GRAVEL, trace silt, occasi ional pieces of broken roc | ional cobbles, | | | 35 | | |] | | | | | | | | | | | | | = |
| <u> </u> | sand | and gravel, sub-rounded t | | | | 57 | | | | | | ÷ | | | | | • | | | | | |
| - | damp | , dense, brown. | | | 2 | 95 | GWS | | 3 | • | 1 | | | | | | | | | | | - 1643.0_ |
| F | | | | | | 73 | | | | | ·· | | | | | | ÷ | | •••••• | | | - 1 |
| E_2 | | | | | | 56 | | |] | | - | 1 | | | | | | | | | | - |
| | SAND grav | elly, some silt, occasional | cobbles well | | | | | مور مان مور مان | | | 1 | ŤŤ | | | | | | | | | | |
| - | grade | d sand, fine gravel, sub-a | ngular to | | | 45 | | | | | | | | | | | | | | | | 1642.0 |
| - | sub-ro | ounded, damp, dense, bro | wn. | | 3 | 40 | SWG | \$ | 5 | • | 1 | | | | | | 1 | | | | | = |
| <u> </u> | | | | | | 74 | | | | | | į., į. | | | | | | | | | | |
| E | SAND, grav mediu | elly, trace silt, occasional im to coarse sand, sub-ro | cobbles, unded to | | | 61 | | 0 | | | i | | | | | | 1 | ı į | | | | = |
| _ | | ar, damp, very dense, bro | | | | 135 | SPG | · • . [| | | <u>.</u> | ļļ. | | | | | .ļļ | | | | | 1641.0 |
| | SAND, grav | elly, occasional pieces of | broken rock. | | 4 | 100 | | in. | 5 | • | | | | | | | | | | | | |
| - 4 | coars | e sand, well graded grave ounded, very wet, very der | l, angular to | | | | SPG | 0 | | | | | | | | | · • · · • | | | | | |
| F | -water enco | untered at 4 m depth | ſ | | | 80 | | 0.00 | | | | | | | | | | | | | | - 1640.0_ |
| - | EOH (open) | at 4.2 m - Refusal (likely | on a boulder) | | | 58 | | | | | | ֠. | | | | | | | | | | _ |
| 5 | | | | | | 55 | | | | | ł | 1 | | | | | • | | | | | _ |
| 0 | | | | | | 62 | | | | | | ŤŤ | | | | | ÷. | r † | | | | - |
| E | | | | | | 51 | | | | | | | | | | | | | | | | 1639.0_ |
| Ē | | | | | | 131 | | | | | | | | | | | | | | | | = |
| E 6 | | | | | | 98 | | | | | <u>.</u> | | | | | | | | | | | |
| E | | | | | | 62 | | | | | | | | | | | | | | | | - |
| _ | | | | | | 72 | | | | ļļ. | | ļ | | | | | | | | | | 1638.0 |
| | | | | | | 63 | | | | | 1 | | | | | | | | | | | - |
| <u> </u> | | | | | | | | | | | | ÷ | | | | | | | | | | |
| _ | | | | | | 58 | | | | | ł | | | | | | | | | | | - 1637.0 |
| - | | | | | | 46 | | | | | | | | | | | | | | | | - |
| E 。 | | | | | | 39 | | | | | 1 | | | | | | • | | | | | |
| E° | | | | | | 49 | | | | 111 | | | | | | | ÷, | | | | | |
| - | | | | | | 54 | | | | | 1 | | | | | | | | | | | 1636.0 |
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| - 9 | | | | | | 68 | | | | | | ļ., | | | , | | | | | | | |
| E | | | | | | 43 | | | | | | | | | | | | | | | | - |
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| Ē | | | | | | 64 | | | | | 1 | | | | | | | | | | | |
| - 10 | | | | | | 58 | | | OGGI | | | | | | : | | | : = T 1/ | | | H: 12 | |
| | 🚓 EBA, A Tetra Tech Col | | | | pa | nv | | | REVIE | | | | V | | | | | | | 6/201 | | JIII |
| | | | | | | ., | | | DRAW | | | | | | | | e1c | | | | | |
| GEOTECHI | NICAL V33101067 BC | REHOLE LOGS (AUGUST 25, 201 | 1).GPJ EBA.GDT 8/25/1 | 1 | | | | | | | | | | | | | | | | | | |

| Trans Canada Highway - Km 81.3 to 85.5 South Side of Highway | | | | Parks Canada Agency | | | | | | | | | F | PROJECT NO BOREHOLE NO. | | | | | NO. | | | | | |
|---|------------------------|-------------------------|-----------------------------|------------------------------|-----------------------|-----|-------------|------------------|----------|----------|-------|-------------------------|----------|-------------------------|-----------|------------|---------------|-----------------|------|---------------|--|--|--|--|
| | - | | | Beck | er Ham | mer | | | | | | | | V | 331(| 0106 | 7 E | BH201 | 1-00 | 6 | | | | |
| N. 570 | 00437.7 E. 5 | 49246.3 | | | | | | | | | | | EL | EVA | TIO | N: 16 | 44.4r | n | | | | | | |
| | PLE TYPE | DISTURBED | NO RECOV | 2 | SPT | | | | -CASI | | | | ELBY " | | | | ORE | | | | | | | |
| BACK | FILL TYPE | BENTONITE | PEA GRAV | | | UGH | | • | ROUT | | | 🛛 DR | LL CU | TTING | SS 🗄 | ះ s | AND | | | | | | | |
| | | | | ы Ж | | | 2 | ENT | | | | | | | | | | | | | | | | |
| Ξ. | | SOIL | | TYPE UMBEI | (P | 0 | MBC | ONT | | | | | | ■B | ECKE | RPEN | IETRAT | TION (Ŋ) 160 | | ш ц | | | | |
| Depth (m) | | DESCRIPT | | ш Z | BPT (N _b) | USC | SΥΙ | R O | <u> </u> | | | | | | 40 UN | 80 CONF | 120 INED (| | _ | atio | | | | |
| ð | | DESCRIPT | | SAMPLE TYPE SAMPLE NUMBER | l m | | SOIL SYMBOL | MOISTURE CONTENT | PLAS | STIC | М. | .C. LIC | UID | | 50 | 100 | 150 | | _ | Elevation (m) | | | | |
| | | | | SAI | | | S | § | | 20 | 40 | 60 | 0 | | 100 | 200 | 300 | | | | | | | |
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| E | | | | | 116 | | | | | | | | | | | | | | | - 1633.0_ | | | | |
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| E 12 | | | | | 216 | | | | | | | | | | | | | | 501 | <u>י</u> | | | | |
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| F | | | | | | | | | | | | | | | | | | | | 1632.0 | | | | |
| E | EOH (closed | d) at 12.5 m | | | | | | | | | | | | | | | | | | - | | | | |
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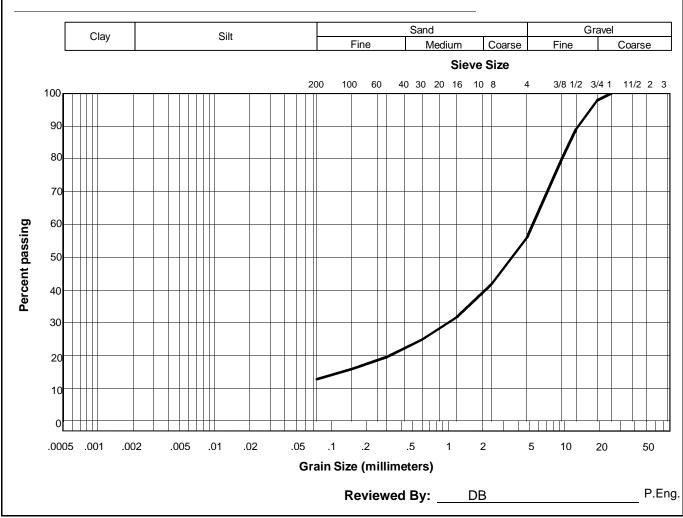
| Trans | Canada Hig | hway - Km 81.3 to 8 | 5.5 | Pa | arks | Canad | a Age | ncy | | | | | | | Ρ | ROJ | ECT | NO | BC | DREH | OLE | NO. |
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| South | Side of High | iway | | Be | ecke | r Hamı | mer | | | | | | | | | V3 | 3310 | 106 | 7 | BH201 | 1-0 | 7 |
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| SAMP | PLE TYPE | DISTURBED | NO RECOV | 'ERY | ′ D | SPT | | | | -CASI | NG | | | SHEL | | | | _ | ORE | | | |
| BACK | FILL TYPE | BENTONITE | PEA GRAV | EL | | SLO | UGH | | | ROUT | - | | \square | DRILL | CUT | TING | s ៃ | ໍ S/ | AND | | | |
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| (E) | | SOIL | | TYPE | M | 9 | | BC | INO | | | | | | | | | | IETRA | TION (N |) 🔳 | m) |
| Depth (m) | | | | Щ | SAMPLE NUMBER | BPT (N _b) | USC | SYMBOL | MOISTURE CONTENT | <u> </u> | | | | | _ | | 40 • UNC | 80 ONF | | | | Elevation (m) |
| Del | | DESCRIPTIO | JIN | SAMPLE | IPL | 6 | | SOIL | STUF | PLAS | STIC | М. | C. | LIQUI | D | | 50 | 100 | 150 | 200 | | leva |
| | | | | Ś | SAN | | | N N |) Ň | | 20 | 40 | 60 | | | | | | PEN. 300 | (kPa) ▲ 400 | • | ш |
| = 0 | SAND and G | GRAVEL, some silt, occa | sional cobbles | | | 11 | | ¢ | | | | | | | | | | | | | | = |
| E | fine g | ieces of broken rock, wel avel, angular to sub-rou | | | | 23 | | |] | | | | | | | | | | | | | - 1644.0 |
| F | compa | act, brown. | | | | 34 | | °.°° | | | | | | | | | | | | | | = |
| E 1 | SAND and | GRAVEL, some silt, occa | sional cobbles | | | 50 | | <i>v</i> | | | | | <u></u> | ļ.ļ. | | | | ļ | | .įį | ļ | _ |
| E | and p | ieces of broken rock, wel ravel, angular to sub-rou | l graded sand, | | | | SWG | ູຄໍໍ | 1 | | | | | | | | | | | | : | - |
| - | | to very dense, brown. | naca, aamp, | | | 73 | | | | . | | | | | | | ÷ | | | | | 1643.0 |
| Ē | | | | | 1 | 89 | | ÷. | | | | | | | | | | - | | | | - |
| <u>2</u> | | | | | 1 | 76 | | . 8. 9 | | | | | | | | | | . 📫 | | · | ÷ | _ |
| _ | | | | | | 47 | |). | | | | | | | | | • | | | | | = |
| | GRAVEL ar | id SAND, trace to some s es and pieces of broken | silt, occasional | 1 | | 34 | | |] | | | | | ÷ | | | Ċ | | | ÷÷ | | 1642.0 |
| E a | grade | d sand and gravel, sub-r | ounded to | | | 60 | | | | | | | | | | | | | | | | - |
| <u> </u> | sub-a brown | ngular, damp, dense to v | ery dense, | | | 570 | GWS | |] | | | | | ÷ | | | ŤŤ | | 1 | | 570 | - |
| Ē | | e recovery from 2.4 to 3. | 7 m depth | | 2 | 3/0 | | | 2 | | | | | | | | | | | | 1 | 1641.0 |
| | EOH (closed | | | | | | | | | | | 1 | | | | | ĪĪ | 1 | | 11 | 1 | |
| E 4 | SAND, grav | elly, some silt, frequent fi k, well graded sand and | ractured pieces gravel, | \square | 3 | | SWG | | ° | | | | | | | | | | | | ļ | - |
| F | | ounded to angular, very v | | | | | | | | | | | | | | | | | | 11 | | - |
| Ē | | untered at 3.7 m depth | | | | | | | | | | | | | | | | | | <u>.</u> | <u>.</u> | 1640.0 |
| E | EOH (open) | at 3.9 m - Refusal (likely | on a boulder) | | | | | | | | | | | | | | | | | | | - |
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GEOTECHNICAL V33101067 BOREHOLE LOGS (AUGUST 25, 2011).GPJ EBA.GDT 8/25/11

APPENDIX D APPENDIX D SIEVE ANALYSES RESULTS



| | GRAIN SIZE DISTRIBUTION | | |
|--------------------|-------------------------------------|--------------------|-----------------|
| | ASTM C136 & C117 | Sieve Size (mm) | Percent Passing |
| Project: Trans C | Canada Highway (TCH) Km 81.3 - 85.5 | 25.000 | 100 |
| Anim | al Underpass Structures | 19.000 | 98 |
| Project Number: | V33101067 | 12.500 | 89 |
| Date Tested: | June 23, 2011 | 9.500 | 80 |
| Borehole Number: | BH2011-01 Sample 1 | 4.750 | 56 |
| Depth: | 0.6 m | 2.360 | 42 |
| Soil Description: | GRAVEL and SAND, some fines | 1.180 | 32 |
| Cu: N/ | Ά | 0.600 | 25 |
| Cc: N/ | Ά | 0.300 | 20 |
| Natural Moisture C | Content: 4.8% | 0.150 | 16 |
| Remarks: Grav | el (44%) Sand (43%) Fines (13%) | 0.075 | 12.8 |





| | GRAIN SIZE DISTRIBUTION | | |
|-------------------|---|--------------------|-----------------|
| | ASTM C136 & C117 | Sieve Size (mm) | Percent Passing |
| Project: Trans | Canada Highway (TCH) Km 81.3 - 85.5 | 37.500 | 100 |
| Anin | nal Underpass Structures | 25.000 | 97 |
| Project Number: | V33101067 | 19.000 | 91 |
| Date Tested: | June 23, 2011 | 12.500 | 80 |
| Borehole Number | r: BH2011-01 Sample 5 | 9.500 | 74 |
| Depth: | 9.4 m | 4.750 | 65 |
| Soil Description: | GRAVEL & SAND, silty* | 2.360 | 60 |
| Cu: N | I/A | 1.180 | 56 |
| Cc: N | I/A | 0.600 | 52 |
| Natural Moisture | Content: 6.9% | 0.300 | 44 |
| Remarks: Grav | vel (35%) Sand (41%) Fines (24%) | 0.150 | 33 |
| *Fine | es description based on visual assessment | 0.075 | 24.4 |

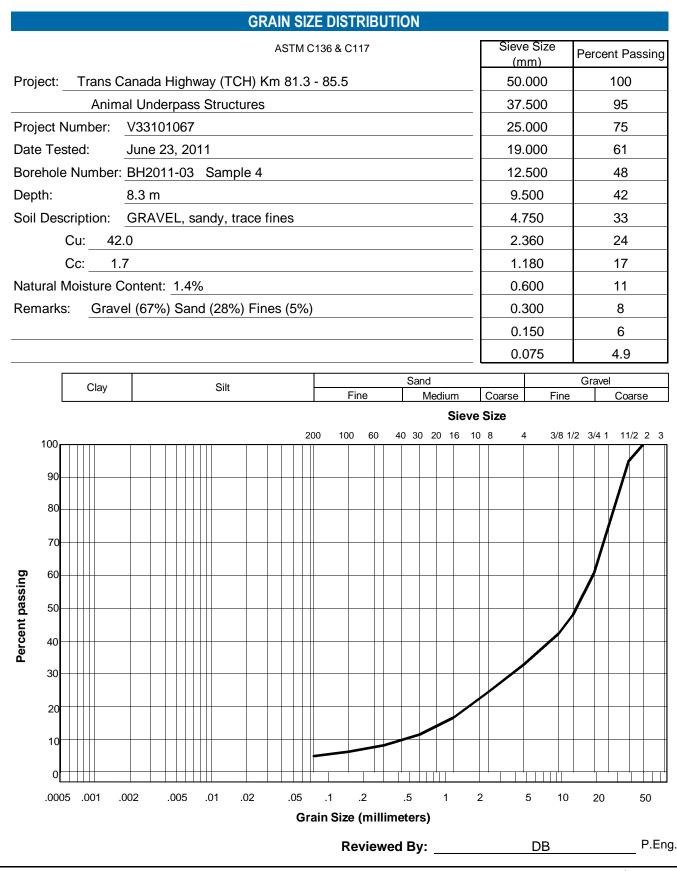




| | GRAIN SIZE DISTRIBUTION | | |
|--------------------|-------------------------------------|--------------------|-----------------|
| | ASTM C136 & C117 | Sieve Size (mm) | Percent Passing |
| Project: Trans C | Canada Highway (TCH) Km 81.3 - 85.5 | 37.500 | 100 |
| Anim | al Underpass Structures | 25.000 | 96 |
| Project Number: | V33101067 | 19.000 | 92 |
| Date Tested: | June 23, 2011 | 12.500 | 89 |
| Borehole Number: | BH2011-03 Sample 2 | 9.500 | 85 |
| Depth: | 4.5 m | 4.750 | 74 |
| Soil Description: | SAND, gravelly, trace fines | 2.360 | 58 |
| Cu: 12 | .8 | 1.180 | 36 |
| Cc: 1. | 7 | 0.600 | 19 |
| Natural Moisture C | Content: 2.7% | 0.300 | 12 |
| Remarks: Grav | el (26%) Sand (67%) Fines (7%) | 0.150 | 9 |
| | | 0.075 | 6.7 |









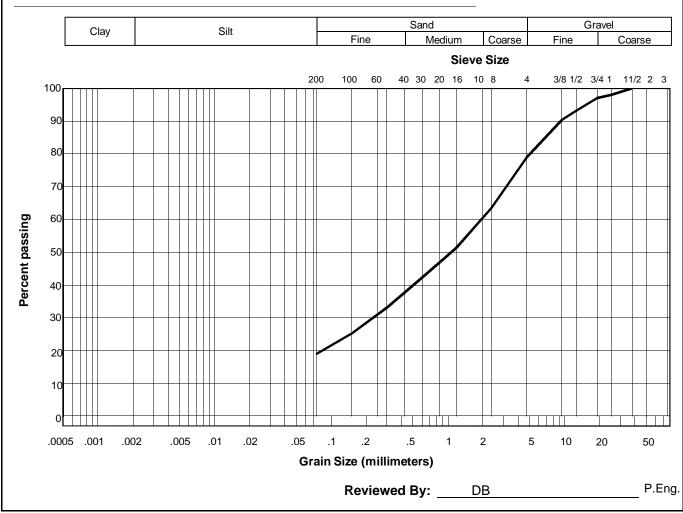
| | GRAIN SIZE DISTRIBUTION | | |
|-------------------|-------------------------------------|------------|-----------------|
| | ASTM C136 & C117 | Sieve Size | Percent Passing |
| Project: Trans (| Canada Highway (TCH) Km 81.3 - 85.5 | 19.000 | 100 |
| Anim | nal Underpass Structures | 12.500 | 100 |
| Project Number: | V33101067 | 9.500 | 99 |
| Date Tested: | June 23, 2011 | 4.750 | 96 |
| Borehole Number | : BH2011-04 Sample 2 | 2.360 | 81 |
| Depth: | 5 m | 1.180 | 47 |
| Soil Description: | SAND, trace gravel, trace fines | 0.600 | 22 |
| Cu: 9 | .6 | 0.300 | 13 |
| Cc: 2 | .2 | 0.150 | 10 |
| Natural Moisture | Content: 2.5% | 0.075 | 7.3 |
| | (40/) Sond (900/) Einon (70/) | | |

Remarks: Gravel (4%) Sand (89%) Fines (7%)



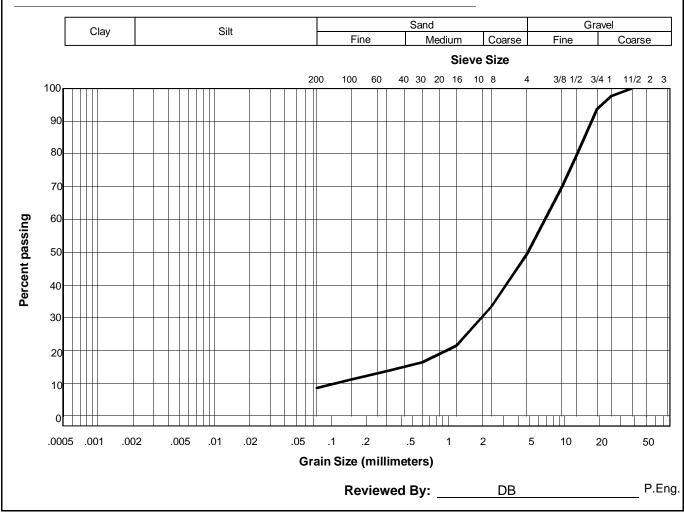


| | GRAIN SIZE DISTRIBUTION | | |
|-------------------|-------------------------------------|--------------------|-----------------|
| | ASTM C136 & C117 | Sieve Size (mm) | Percent Passing |
| Project: Trans | Canada Highway (TCH) Km 81.3 - 85.5 | 37.500 | 100 |
| Anin | nal Underpass Structures | 25.000 | 98 |
| Project Number: | V33101067 | 19.000 | 97 |
| Date Tested: | June 23, 2011 | 12.500 | 93 |
| Borehole Number | r: BH2011-04 Sample 4 | 9.500 | 90 |
| Depth: | 7.6 m | 4.750 | 79 |
| Soil Description: | SAND, gravelly, some fines | 2.360 | 64 |
| Cu: N | I/A | 1.180 | 51 |
| Cc: N | I/A | 0.600 | 42 |
| Natural Moisture | Content: 5.9% | 0.300 | 33 |
| Remarks: Grav | vel (21%) Sand (60%) Fines (19%) | 0.150 | 25 |
| | | 0.075 | 19.0 |





| | GRAIN SIZE DISTRIBUTION | | |
|-------------------|-------------------------------------|--------------------|-----------------|
| | ASTM C136 & C117 | Sieve Size (mm) | Percent Passing |
| Project: Trans (| Canada Highway (TCH) Km 81.3 - 85.5 | 37.500 | 100 |
| Anim | nal Underpass Structures | 25.000 | 98 |
| Project Number: | V33101067 | 19.000 | 94 |
| Date Tested: | June 23, 2011 | 12.500 | 79 |
| Borehole Number | : BH2011-05 Sample 2 | 9.500 | 70 |
| Depth: | 3 m | 4.750 | 50 |
| Soil Description: | GRAVEL and SAND, trace fines | 2.360 | 33 |
| Cu: 61 | 1.9 | 1.180 | 21 |
| Cc: 5 | .0 | 0.600 | 16 |
| Natural Moisture | Content: 5.9% | 0.300 | 14 |
| Remarks: Grav | vel (50%) Sand (41%) Fines (9%) | 0.150 | 11 |
| | | 0.075 | 8.5 |





| GRAIN SIZE DISTRIBUTION | | | |
|-------------------------------------|-------------------------------------|--------------------|-----------------|
| | ASTM C136 & C117 | Sieve Size (mm) | Percent Passing |
| Project: Trans | Canada Highway (TCH) Km 81.3 - 85.5 | 37.500 | 100 |
| Animal Underpass Structures | | 25.000 | 96 |
| Project Number: | V33101067 | 19.000 | 94 |
| Date Tested: | June 23, 2011 | 12.500 | 85 |
| Borehole Number: BH2011-06 Sample 3 | | 9.500 | 80 |
| Depth: | 2.6 m | 4.750 | 66 |
| Soil Description: | SAND, gravelly, some fines | 2.360 | 52 |
| Cu: N/A | | 1.180 | 39 |
| Cc: N/A | | 0.600 | 31 |
| Natural Moisture Content: 5.0% | | 0.300 | 26 |
| Remarks: Grav | vel (34%) Sand (48%) Fines (18%) | 0.150 | 22 |
| | | 0.075 | 17.9 |

